



**COLLEGE OF ENGINEERING
PUTRAJAYA CAMPUS
FINAL EXAMINATION
SEMESTER 2 2011 / 2012**

PROGRAMME : Bachelor of Electrical & Electronics Engineering (Honours)
Bachelor of Electrical Power Engineering (Honours)

SUBJECT CODE : EEEB273

SUBJECT : ELECTRONIC ANALYSIS AND DESIGN II

DATE : January 2012

TIME : 3 hours (9.00 am – 12.00 pm)

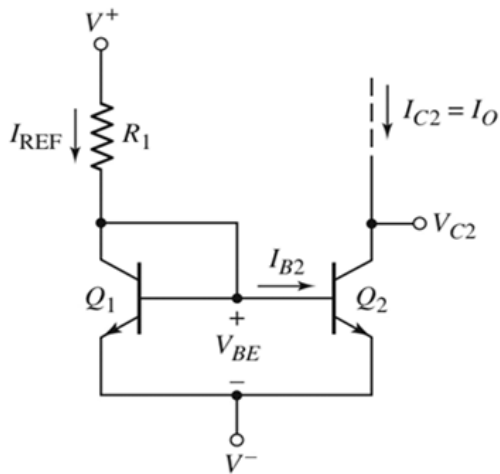
INSTRUCTIONS TO CANDIDATES:

1. This question paper contains SIX (6) questions in TWELVE (12) pages.
2. Answer **ALL** questions.
3. Write **all** answers in the answer booklet provided.
4. Write answer to each question on a **new page**.
5. For all calculations, assume that $V_T = 26 \text{ mV}$.

MODEL ANSWER

***THIS QUESTION PAPER CONSISTS OF TWELVE (12) PRINTED PAGES INCLUDING
THIS COVER PAGE AND APPENDIX.***

Q1(a)(i)



Transistors	[1]
I_{REF}	[0.5]
R_1	[0.5]
I_O	[0.5]
Connection	[0.5]
Total	[3 marks]

Q1(a)(ii)

$$I_{REF} = I_{S1} e^{V_{BE1}/V_T}$$

1

$$V_{BE1} = V_T \ln\left(\frac{I_{REF}}{I_{S1}}\right)$$

1

$$V_{BE1} = 0.026 \ln\left(\frac{210\mu}{4.5 \times 10^{-15}}\right) = 0.6387V$$

0.5, 0.5

$$V_{BE2} = V_{BE1} = 0.6387V$$

$$I_O = I_{S2} e^{V_{BE2}/V_T}$$

1

$$I_O = 3 \times 10^{-15} e^{0.6387/0.026} = 139.9\mu A$$

0.5, 0.5

Q1(b)(i)

Identical transistors, therefore aspect ratios are the same

$$I_D = \frac{k'_n}{2} \left(\frac{W}{L} \right) [V_{GS} - V_{TN}]^2 \quad \boxed{1}$$

$$V_{GS} - V_{TN} = V_{DS}(\text{sat}) = 0.8\text{V} \quad \boxed{1}$$

$$\frac{W}{L} = \frac{2I_D}{k'_n [V_{DS}(\text{sat})]^2} \quad \boxed{1}$$

$$\frac{W}{L} = \frac{2(1\text{m})}{(120\mu)(0.8)^2} = 26.04 \quad \boxed{0.5, 0.5}$$

Q1(b)(ii)

$$R = \frac{V^+ - V^+ - 2V_{GS}}{I_D} \quad \boxed{1}$$

$$V_{GS} = V_{DS}(\text{sat}) + V_{TN} = 0.8 + 1.5 = 2.3\text{V} \quad \boxed{0.5}$$

$$R = \frac{15 - (-15) - 2(2.3)}{1\text{m}} = 25.4\text{k}\Omega \quad \boxed{0.5}$$

Q1(b)(iii)

$$R_o = \frac{1}{\lambda I_D} = \frac{1}{(0)I_D} = \infty \quad \boxed{1}$$

$$\Delta I_o = \frac{\Delta V}{R_o} = \frac{\Delta V}{\infty} = 0 \quad \boxed{1}$$

Therefore, no change in current

Q2(a)

$$I_1 = I_Q = 2I_{D1} = 2(60\mu) = 120\mu\text{A} \quad \boxed{1}$$

$$V_{DS5} = V_{DS3} = V_{GS3} = V_{GS4} = \sqrt{\frac{I_Q}{K_{n4}}} + V_{TN} = \sqrt{\frac{120\mu}{100\mu}} + 0.3 = 1.3954\text{V} \quad \boxed{2}$$

$$R_1 = \frac{V^+ - V_{DS5} - V_{DS3} - V^-}{I_1} = \frac{3 - 1.3954 - 1.3954 - (-3)}{120\mu} = 26.74\text{k}\Omega \quad \boxed{1.5}$$

$$I_{D1} = K_{n1}(V_{GS1} - V_{TN})^2 \Rightarrow V_{GS1} = \sqrt{\frac{I_{D1}}{K_{n1}}} + V_{TN} = \sqrt{\frac{60\mu}{150\mu}} + 0.3 = 0.9324\text{V} \quad \boxed{1.5}$$

$$R_D = \frac{V^+ - V_{D1}}{I_{D1}} = \frac{V^+ - (V_{DS1} + V_{S1})}{I_{D1}} = \frac{V^+ - (V_{DS1} + V_{G1} - V_{GS1})}{I_{D1}} \quad \boxed{1}$$

$$R_D = \frac{V^+ - V_{DS1} - v_1 + V_{GS1}}{I_{D1}} = \frac{3 - 3 - (-0.5) + 0.9324}{60\mu} = 23.87\text{k}\Omega \quad \boxed{1}$$

Q2(b)

$$R_o \cong g_{m4}r_{o4}r_{o6} = 2\sqrt{K_{n4}I_Q} \frac{1}{\lambda_4 I_Q} \frac{1}{\lambda_6 I_Q} \quad \boxed{1}$$

$$R_o = 2\sqrt{(100\mu)(120\mu)} \frac{1}{0.01(120\mu)} \frac{1}{0.01(120\mu)} = 152.03\text{M}\Omega \quad \boxed{1}$$

$$A_d = \frac{g_{m2}R_D}{2} \quad \boxed{0.5}$$

$$g_{m2} = 2\sqrt{K_{n2}I_{D2}} = 2\sqrt{(150\mu)(60\mu)} = 189.73\mu\text{A/V} \quad \boxed{0.5}$$

$$A_d = \frac{(189.73\mu)(23.87\text{k})}{2} = 2.26 \quad \boxed{1}$$

$$A_{cm} = -\frac{g_{m2}R_D}{1 + 2g_{m2}R_o} \quad \boxed{1}$$

$$A_{cm} = -\frac{(189.73\mu)(23.87\text{k})}{1 + 2(189.73\mu)(152.03\text{M})} = -8.08 \times 10^{-6} \quad \boxed{1}$$

$$\text{CMRR} = \left| \frac{A_d}{A_{cm}} \right| = \left| \frac{2.26}{-8.08 \times 10^{-6}} \right| = 279502.44 \quad \boxed{2}$$

Q3(a)

$$v_o = A_v v_d \quad \boxed{1}$$

$$A_v = g_{m2}(r_{o2} \parallel R_o) \quad \boxed{1}$$

$$r_{o2} = \frac{1}{\lambda_n I_{D2}} = \frac{1}{(0.02)(100\mu)} = 500\text{k}\Omega \quad \boxed{1}$$

$$R_o \cong g_{m4} r_{o4} r_{o6} \quad \boxed{1}$$

$$r_{o4} = r_{o6} = \frac{1}{\lambda_p I_{D4}} = \frac{2}{\lambda_p I_Q} \quad \boxed{0.5}$$

$$r_{o4} = r_{o6} = \frac{2}{(0.03)(200\mu)} = 333.3\text{k}\Omega \quad \boxed{0.5}$$

$$g_{m4} = 2\sqrt{\frac{k'_p}{2} \left(\frac{W}{L}\right)_p I_{D2}} = \sqrt{k'_p \left(\frac{W}{L}\right)_p I_Q} \quad \boxed{0.5}$$

$$g_{m4} = \sqrt{(50\mu)(12)(200\mu)} = 0.3464\text{mA/V} \quad \boxed{0.5}$$

$$R_o = (0.3464\text{m})(333.3\text{k})(333.3\text{k}) = 38.5\text{M}\Omega$$

$$r_{o2} \parallel R_o \cong r_{o2} = 500\text{k}\Omega \quad \boxed{0.5}$$

$$g_{m2} = \sqrt{k'_n \left(\frac{W}{L}\right)_n I_Q} = \sqrt{(100\mu)(10)(200\mu)} = 0.4472\text{mA/V} \quad \boxed{0.5}$$

$$v_o = A_v v_d = g_{m2} r_{o2} v_d \quad \boxed{1}$$

$$v_o = (0.4472\text{m})(500\text{k})(20\sin\alpha)\mu = 4.472\sin\alpha(\text{mV})$$

Q3(b)(i)

- Differential amp circuit [0.5]
- 3-transistor active load circuit [0.5]
- Darlington pair circuit OR gain circuit [0.5]
- Output stage [0.5]

Q3(b)(ii)

Reflection rule

$$R_i = r_{\pi 6} + (1 + \beta)r_{\pi 7}$$

1

$$\beta = g_m r_{\pi 6}$$

1

$$\beta = (5\text{m})(3\text{k}) = 15$$

1

$$R_i = 3\text{k} + (1 + 15)(3\text{k}) = 51\text{k}\Omega$$

$$R_o = R_2 \parallel \frac{r_{\pi 8} + r_{o7} \parallel r_{o11}}{(1 + \beta)}$$

1

$$R_o = 10\text{k} \parallel \frac{3\text{k} + 500\text{k} \parallel 500\text{k}}{(1 + 15)} = 6.125\text{k}\Omega$$

1, 1

Q4(a)(i)

$$R_5 = \frac{V^+ - V_{EB12} - V_{BE11} - V^-}{I_{REF}} \quad \boxed{0.5}$$

$$V_{EB12} = V_{BE11} = V_T \ln \frac{I_{REF}}{I_S} = 0.026 \ln \frac{1 \times 10^{-3}}{10^{-14}} = 0.658 \text{V} \quad \boxed{1.5}$$

$$R_5 = \frac{15 - 0.658 - 0.658 - (-15)}{1 \text{m}} = 28.68 \text{k}\Omega \quad \boxed{0.5}$$

$$I_{C10} = I_{C9} = 10 \times 10^{-6} \text{A} \quad \boxed{0.5}$$

$$R_4 = \frac{V_T}{I_{C10}} \ln \frac{I_{REF}}{I_{C10}} = \frac{0.026}{10 \times 10^{-6}} \ln \frac{1 \times 10^{-3}}{10 \times 10^{-6}} = 11.97 \text{k}\Omega \quad \boxed{1}$$

Q4(a)(ii)

$$I_{C1} = \frac{I_{C8}}{2} = \frac{I_{C9}}{2} = \frac{10 \mu\text{A}}{2} = 5 \mu\text{A} \quad \boxed{1}$$

$$r_{\pi 6} = \frac{\beta V_T}{I_{C6}} = \frac{200 \times 0.026}{5 \mu} = 1.04 \text{M}\Omega \quad \boxed{1}$$

Q4(a)(iii)

$$V_{C5} = V_{BE7} + V_{BE6} + I_{C6} R_2 + V^- \quad \boxed{1}$$

$$V_{C5} = 0.6 + 0.6 + (5 \mu\text{A})(1 \text{k}\Omega) + (-15) = -13.795 \text{V} \quad \boxed{1}$$

Q4(b)(i)

$$I_Q = I_{D6} = I_{D5} \quad \boxed{0.5}$$

$$I_{D5} = K_p (V_{SG5} + V_{TP})^2 = (100\mu\text{A}/\text{V}^2) \times (1.5 - 0.5)^2 = 100\mu\text{A} \quad \boxed{1}$$

$$\Rightarrow I_Q = I_{D5} = 100\mu\text{A} = 0.1\text{mA} \quad \boxed{0.5}$$

Q4(b)(ii)

$$A_v = A_d A_{v2} \quad \boxed{0.5}$$

$$A_d = g_m (r_{o2} \parallel r_{o4}) \quad \boxed{0.5}$$

$$g_m = \sqrt{2K_p I_Q} = \sqrt{2(100\mu)(100\mu)} = 141.42\mu\text{A}/\text{V} \quad \boxed{0.5}$$

$$r_{o2} = \frac{1}{\lambda_p I_{D2}} = \frac{1}{0.02 \times 50\mu} = 1\text{M}\Omega \quad \boxed{0.5}$$

$$r_{o4} = \frac{1}{\lambda_n I_{D4}} = \frac{1}{0.01 \times 50\mu} = 2\text{M}\Omega \quad \boxed{0.5}$$

$$A_d = (141.42\mu)(1\text{M} \parallel 2\text{M}) = 94.286 \quad \boxed{0.5}$$

$$A_{v2} = g_{m7} (r_{o7} \parallel r_{o8}) \quad \boxed{0.5}$$

$$g_m = 2\sqrt{K_{n7} I_{D7}} = 2\sqrt{(125\mu)(100\mu)} = 223.6\mu\text{A}/\text{V} \quad \boxed{0.5}$$

$$r_{o7} = \frac{1}{\lambda_n I_{D7}} = \frac{1}{0.01 \times 100\mu} = 1\text{M}\Omega \quad \boxed{0.5}$$

$$r_{o8} = \frac{1}{\lambda_p I_{D8}} = \frac{1}{0.02 \times 100\mu} = 0.5\text{M}\Omega \quad \boxed{0.5}$$

$$A_{v2} = (223.6\mu)(1\text{M} \parallel 0.5\text{M}) = 74.53 \quad \boxed{0.5}$$

$$A_v = A_d A_{v2} = 94.286 \times 74.53 = 7027.45 \quad \boxed{0.5}$$

Q5(a)

- **Class A:** Output transistor is *biased at a quiescent current I_Q* and conducts for the *entire cycle of the input signal.*

[2]

- **Class B:** Output transistor conducts for only *one-half of each sine-wave input cycle.*

[1]

- **Class AB:** Output transistor biased *at a small quiescent current I_Q* , and conducts for *slightly more than half a cycle.*

[2]

- **Class C:** Output transistors conducts for *less than half a cycle.*

[1]

Q5(b)

$$v_o(\text{max}) = V^+ - V_{CE}(\text{sat}) = 10 - 0.4 = 9.6\text{V}$$

1

$$I_Q = |-i_L(\text{max})| = \frac{v_o(\text{max})}{R_L} = \frac{9.6}{5\text{k}} = 1.92\text{mA}$$

1

$$I_1 = I_Q = \frac{8 - V_{BE}(\text{on}) - V^-}{R}$$

1

$$R = \frac{8 - 0.7 - (-10)}{1.92\text{m}} = 9.01\text{k}\Omega$$

1

$$\eta = \frac{P_L}{P_S} = \frac{(1/2)(i_L(\text{max}))^2 R_L}{I_Q(V^+ - V^-) + I_1(8 - V^-)}$$

1

1

1

$$\eta = \frac{(1/2)(1.92\text{m})^2(5\text{k})}{(1.92\text{m})(20) + (1.92\text{m})(18)} = \frac{9.216\text{mW}}{72.96\text{mW}}$$

1

1

$$\eta = 0.1263 @ 12.63\%$$

1

Question 6 [20 marks]

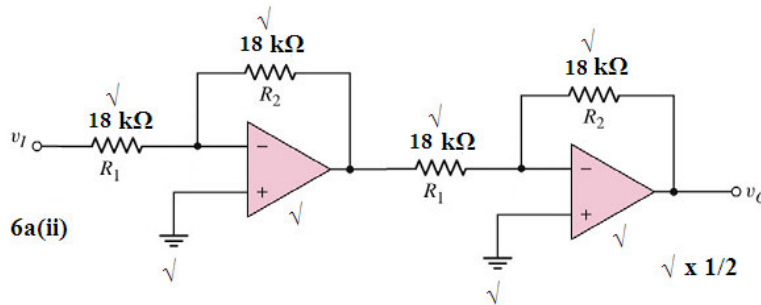
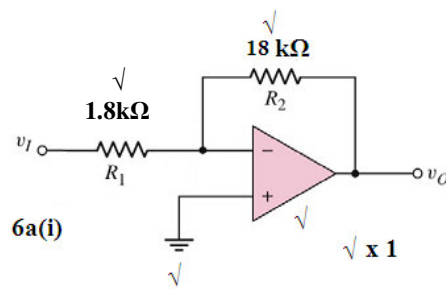
(a) Using **feedback resistor** of **18 kΩ**, draw the following circuits using **inverting op-amp** configuration:

(i) An **inverting amplifier** with a closed-loop gain of **-10**.

[4 marks]

(ii) A **voltage follower**.

[4 marks]



(b) Consider the **non-inverting op-amplifier** shown in **Figure 6a**. Assume the op-amp is ideal. Determine the resistor values of **R₁** and **R₂** to produce a closed-loop gain of **15**, with the minimum resistance in the circuit is to be **20 kΩ**.

[4 marks]

$$A_v = 1 + R_2/R_1 = 15 \quad [1]$$

$$R_2/R_1 = 15 - 1 = 14 \rightarrow R_2 = 14 R_1 \quad [1]$$

$$\text{Select } R_1 = 20 \text{ k}\Omega, \quad [1]$$

$$\text{Then } R_2 = 14 \times 20 \text{ k}\Omega = 280 \text{ k}\Omega \quad [1]$$

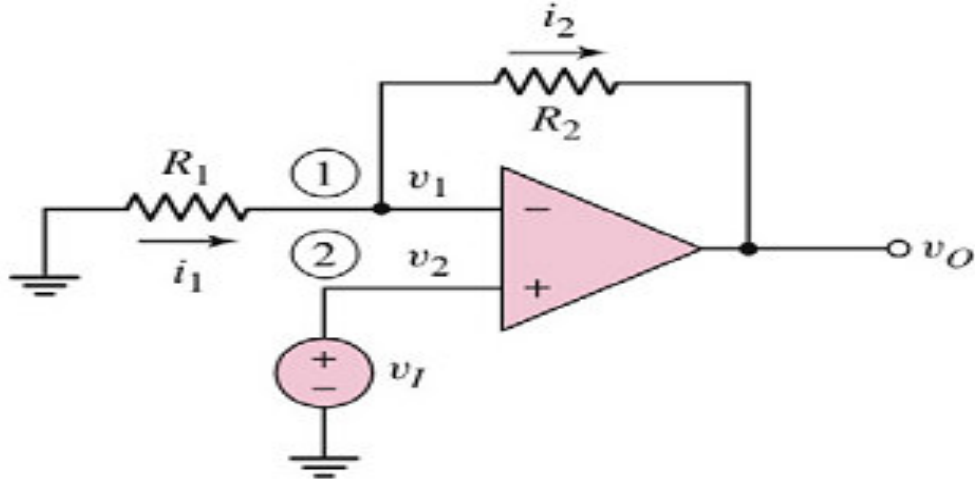


Figure 6a

(c) For a **generalized summing op-amp** as shown in **Figure 6b** the total output voltage is the sum of the individual terms, or

$$v_O = -\frac{R_F}{R_1} v_{I1} - \frac{R_F}{R_2} v_{I2} + \left(1 + \frac{R_F}{R_N}\right) \left(\frac{R_P}{R_A} v_{I3} + \frac{R_P}{R_B} v_{I4}\right)$$

where

$$R_N = R_1 \parallel R_2$$

$$R_P = R_A \parallel R_B \parallel R_C$$

Design a summing op-amp similar to **Figure 6b** to produce the output

$$v_O = -5v_{I1} - 10v_{I2} + 5v_{I3} + 2v_{I4}$$

The smallest resistor value allowable in the design is **15 kΩ**.

[8 marks]

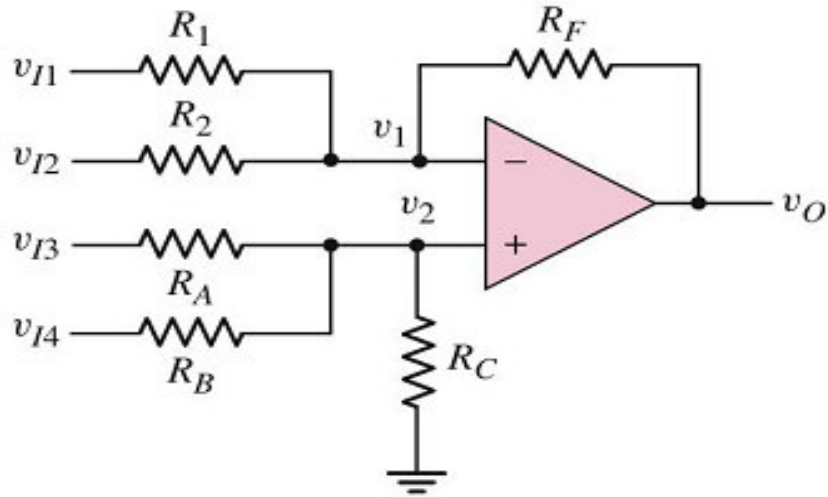


Figure 6b

$$R_F / R_1 = 5 \quad \rightarrow \quad R_F = 5 R_1 \quad [0.5]$$

and $R_F / R_2 = 10 \quad \rightarrow \quad R_F = 10 R_2 \quad [0.5]$

So, resistor R_2 will be the **smallest** value. Set $R_2 = 15 \text{ k}\Omega$. [1]

$\rightarrow \quad R_F = 10 R_2 = 10 \times 15 \text{ k}\Omega = 150 \text{ k}\Omega \quad [0.5]$

and $R_1 = R_F / 4 = 150 \text{ k}\Omega / 5 = 30 \text{ k}\Omega \quad [0.5]$

$$R_N = R_1 \parallel R_2 = 30 \text{ k}\Omega \parallel 15 \text{ k}\Omega = 10 \text{ k}\Omega$$

$$1 + R_F / R_N = 1 + 150 \text{ k} / (10 \text{ k}) = 16$$

$$(1 + R_F / R_N)(R_P / R_A) = (16)(R_P / R_A) = 5 \quad [0.5]$$

and $(1 + R_F / R_N)(R_P / R_B) = (16)(R_P / R_B) = 2 \quad [0.5]$

So, $(R_A / R_B) = 2/5$. [0.5]

Choose $R_A = 80 \text{ k}\Omega$, [1]

then $R_B = 200 \text{ k}\Omega$ [1]

and $R_P = 25 \text{ k}\Omega$ [0.5]

$$R_C = 44.45 \text{ k}\Omega \quad [1]$$

-END OF QUESTION PAPER-