

Name:

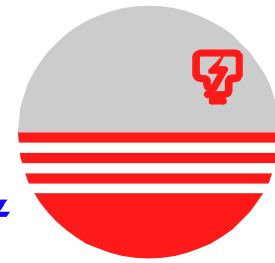
Student ID Number:

Section: 01/02/03 A/B

Lecturer: Dr Jamaludin /

Mdm Jehana Ermy

**UNIVERSITI
TENAGA
NASIONAL**



College of Engineering
Department of Electronics and Communication Engineering

Test 2

SEMESTER 2, ACADEMIC YEAR 2013/2014

Subject Code : **EEEB273**
Course Title : **Electronics Analysis & Design II**
Date : **19 December 2013**
Time Allowed : **1 hour 15 minutes**

Instructions to the candidates:

1. Write your Name and Student ID number. Circle your section number.
2. **Write all your answers using pen. DO NOT USE PENCIL** except for the diagram.
3. **ANSWER ALL QUESTIONS.**
4. **WRITE YOUR ANSWER ON THIS QUESTION PAPER.**
5. For BJT, use $V_T = 26 \text{ mV}$ where appropriate.
6. Use at least **4 significant numbers** in all calculations.

NOTE: DO NOT OPEN THE QUESTION PAPER UNTIL INSTRUCTED TO DO SO.



GOOD LUCK!



Question No.	1	2	Total
Marks			

Question 1 [50 marks]

A MOSFET differential amplifier in **Figure 1(a)** is to be redesigned to use a **P-MOSFET cascode** current source, as shown in **Figure 1(b)**, as an **active load** to replace the drain resistances (R_D). The supply voltages for the overall circuit are $V^+ = 10\text{ V}$ and $V^- = -10\text{ V}$. Bias current for the differential amplifier is $I_Q = 0.3\text{ mA}$. The transistor parameters for the MOSFET differential amplifier pair are $k'_n = 80\text{ }\mu\text{A/V}^2$, $\lambda_n = 0.015\text{ V}^{-1}$ and $V_{TN} = 1\text{ V}$. For all P-MOSFET transistors in the active load, i.e. M_{11} to M_{14} , assume $K_p = 0.1\text{ mA/V}^2$, $\lambda_p = 0.02\text{ V}^{-1}$ and $V_{TP} = -1\text{ V}$.

- (i) **Design** the differential amplifier to achieve a differential-mode voltage gain of $A_d = 400$, where its output v_O is a **one-sided output**. **Show clearly all your calculations. State clearly** all your assumptions, **if any**. Hints: You need to calculate the value of R_O also. [40 marks]
- (ii) **Calculate** output v_O if $v_1 = +0.51\text{ mV}$ and $v_2 = -0.23\text{ mV}$. [10 marks]

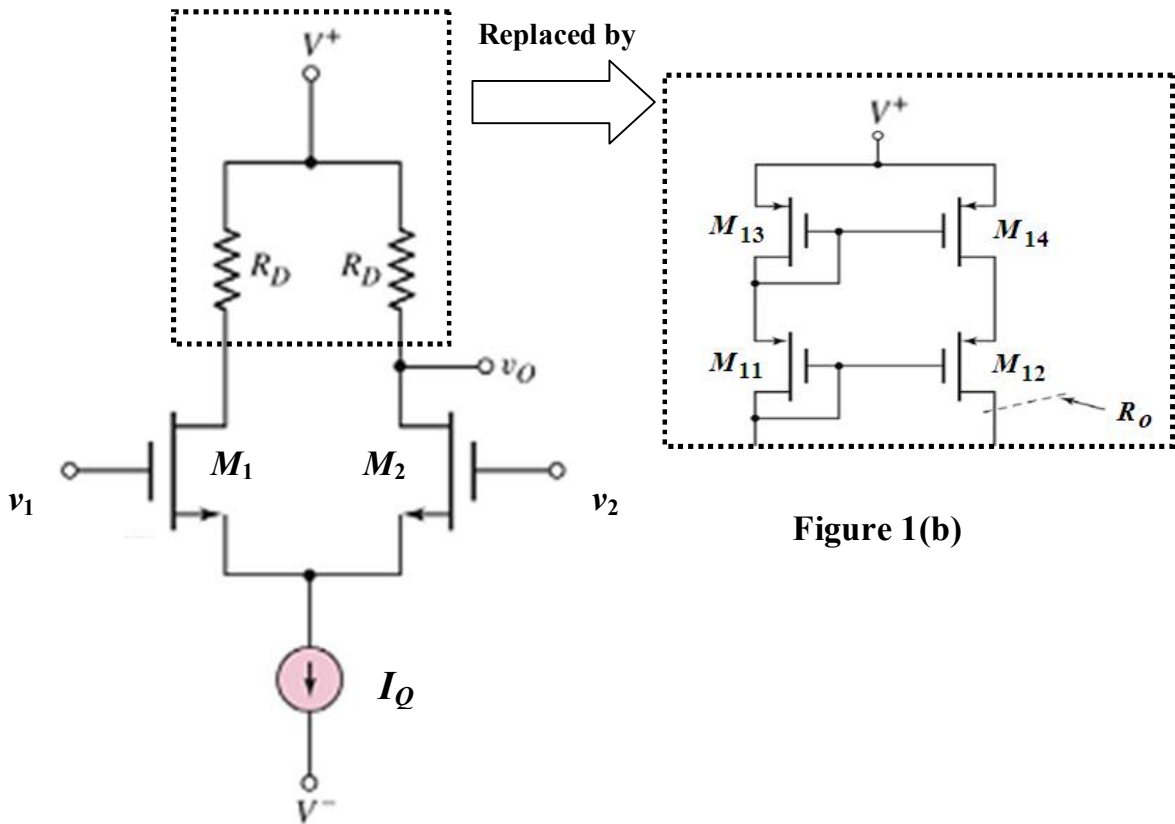


Figure 1(a)

Figure 1(b)

Answers for Question 1

$$(i) A_d = g_{m2}(r_{o2} \parallel R_O) \quad \boxed{3}$$

$$r_{o2} = \frac{1}{\lambda_n \frac{I_Q}{2}} = \frac{1}{0.015(0.15m)} = 444.4k\Omega \quad \boxed{3}$$

$$R_O = g_{m12} r_{o12} r_{o14} \quad \boxed{3}$$

$$g_{m12} = 2\sqrt{K_{p12} I_{D12}} = 2\sqrt{(0.1m) \frac{0.3m}{2}} = 0.2449mA/V \quad \boxed{3}$$

$$r_{o12} = r_{o14} = \frac{1}{\lambda_p \frac{I_Q}{2}} = \frac{1}{(0.02) \frac{0.3m}{2}} = 333.33k\Omega \quad \boxed{4}$$

$$R_O = (0.2449m)(333.33k)(333.33k) = 27.211M\Omega \quad \boxed{3}$$

$$\text{Solution1: } R_O \gg r_{o2} \Rightarrow r_{o2} \parallel R_O \cong r_{o2} \quad \boxed{3}$$

$$A_d = g_{m2}(r_{o2} \parallel R_O) \cong g_{m2} r_{o2} \quad \boxed{3}$$

$$g_{m2} = A_d / r_{o2} = 400 / 444.4k = 0.9mA/V \quad \boxed{3}$$

$$g_{m2} = 2\sqrt{K_{n2} I_{D2}} = 2\sqrt{\frac{k'_n}{2} (W/L)_2 \frac{I_Q}{2}} \quad \boxed{3}$$

$$0.9m = 2\sqrt{\frac{80\mu}{2} (W/L)_2 \frac{0.3m}{2}} \quad \boxed{3}$$

$$(W/L)_2 = \frac{(0.9m)^2}{(80\mu)(0.3m)} = 33.75 \quad \boxed{3}$$

$$(W/L)_1 = (W/L)_2 = 33.75 \quad \boxed{3}$$

$$\text{Solution2: } r_{o2} \parallel R_O = 444.4k \parallel 27.211M = 437.26k \quad \boxed{3}$$

$$A_d = g_{m2}(r_{o2} \parallel R_O) \quad \boxed{3}$$

$$g_{m2} = A_d / (r_{o2} \parallel R_O) = 400 / 437.26k = 0.9147mA/V \quad \boxed{3}$$

$$g_{m2} = 2\sqrt{K_{n2} I_{D2}} = 2\sqrt{\frac{k'_n}{2} (W/L)_2 \frac{I_Q}{2}} \quad \boxed{3}$$

$$0.9147m = 2\sqrt{\frac{80\mu}{2} (W/L)_2 \frac{0.3m}{2}} \quad \boxed{3}$$

$$(W/L)_2 = \frac{(0.9147m)^2}{(80\mu)(0.3m)} = 34.86 \quad \boxed{3}$$

$$(W/L)_1 = (W/L)_2 = 34.86 \quad \boxed{3}$$

Answers for Question 1 (Cont.)

(ii)

$$v_d = v_1 - v_2 = 0.51m - (-0.23m) = 0.74mV$$

3, 2

$$A_d = v_o / v_d$$

$$v_o = A_d v_d = 400(0.74m) = 296mV$$

3, 2

Question 2 [50 marks]

(a) For the circuit shown in **Figure 2(a)**, the transistor parameters are $\beta = 100$ and $V_A = \infty$. The bias currents in the transistors are indicated on the figure. **Determine** the output resistance R_O of the output stage. Show clearly all your calculations.

[20 marks]

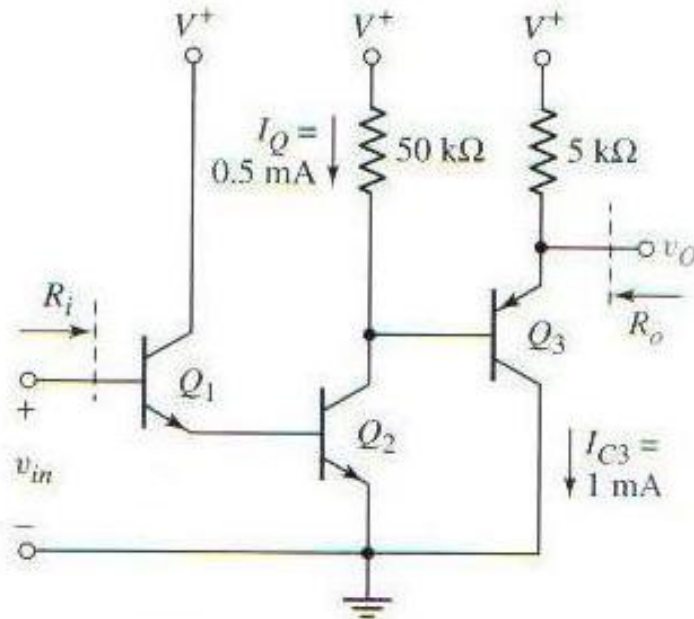


Figure 2(a)

Answers for Question 2(a)

$$R_O = 5k \parallel \frac{r_{\pi 3} + Z}{1 + \beta} \quad \boxed{3}$$

$$Z = 50k \parallel R_{C2} \quad \boxed{3}$$

$$R_{C2} = r_{o2} = V_{A2} / I_{C2} = \infty / (0.5m) = \infty \quad \boxed{5}$$

$$Z = 50k \parallel \infty = 50k\Omega \quad \boxed{2}$$

$$r_{\pi 3} = \beta V_T / I_{C3} = 100(.026) / (1m) = 2.6k\Omega \quad \boxed{4}$$

$$R_O = 5k \parallel \frac{2.6k + 50k}{1 + 100} = 0.472k\Omega \quad \boxed{3}$$

- (b) Study **Figure 2(b)** carefully. The transistor parameters are: $\beta = 180$, $V_{BE(\text{on})} = 0.7 \text{ V}$, and $V_{CE(\text{sat})} = 0.4 \text{ V}$. **Design** the output stage amplifier for maximum output swing and then calculate its **power conversion efficiency**, η . Show clearly all your calculations.

[30 marks]

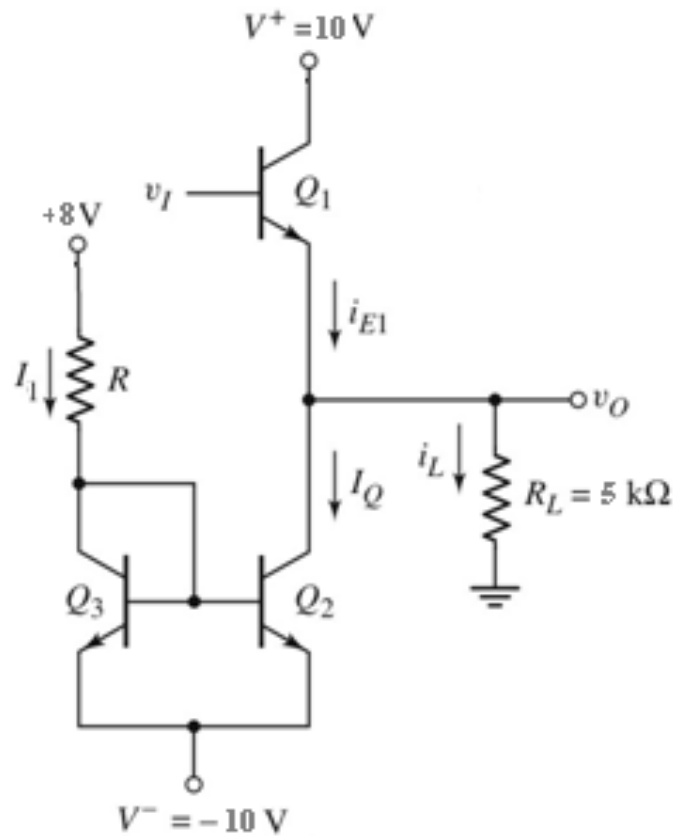


Figure 2(b)

Answers for Question 2(b)

Answers for Question 2(b) (Cont.)

$$v_O(\text{min}) = V^- + V_{CE}(\text{sat}) = -10 + 0.4 = -9.6\text{V}$$

3

$$I_Q = |i_L(\text{min})| = \left| \frac{v_O(\text{min})}{R_L} \right| = \frac{9.6}{5\text{k}} = 1.92\text{mA}$$

3

$$I_1 = I_Q = \frac{8 - V_{BE}(\text{on}) - V^-}{R}$$

3

$$R = \frac{8 - 0.7 - (-10)}{1.92\text{m}} = 9.01\text{k}\Omega$$

3

$$\eta = \frac{P_L}{P_S}$$

3

$$\overline{P}_L = (1/2)(i_L(\text{max}))^2 R_L$$

3

$$\overline{P}_L = (1/2)(1.92\text{m})^2 (5\text{k}) = 9.216\text{mW}$$

3

Solution1 :

$$\overline{P}_S = I_Q(V^+ - V^-) + I_1(8 - V^-)$$

3

$$\overline{P}_S = (1.92\text{m})(20) + (1.92\text{m})(18) = 72.96\text{mW}$$

3

$$\eta = \frac{9.216\text{mW}}{72.96\text{mW}} = 0.1263 @ 12.63\%$$

3

Solution2 :

$$\overline{P}_S = I_Q(V^+ - V^-)$$

3

$$\overline{P}_S = (1.92\text{m})(20) = 38.4\text{mW}$$

3

$$\eta = \frac{9.216\text{mW}}{38.4\text{mW}} = 0.24 @ 24\%$$

3

Appendix: BASIC FORMULA

BJT

$$i_C = I_S e^{v_{BE}/V_T}; \text{npn}$$

$$i_C = I_S e^{v_{EB}/V_T}; \text{pnp}$$

$$i_C = \alpha i_E = \beta i_B$$

$$i_E = i_B + i_C$$

$$\alpha = \frac{\beta}{\beta + 1}$$

;Small signal

$$\beta = g_m r_\pi$$

$$r_\pi = \frac{\beta V_T}{I_{CQ}}$$

$$g_m = \frac{I_{CQ}}{V_T}$$

$$r_o = \frac{V_A}{I_{CQ}}$$

MOSFET

;N – MOSFET

$$v_{DS}(\text{sat}) = v_{GS} - V_{TN}$$

$$i_D = K_n [v_{GS} - V_{TN}]^2$$

$$K_n = \frac{k'_n}{2} \cdot \frac{W}{L}$$

;P – MOSFET

$$v_{SD}(\text{sat}) = v_{SG} + V_{TP}$$

$$i_D = K_p [v_{SG} + V_{TP}]^2$$

$$K_p = \frac{k'_p}{2} \cdot \frac{W}{L}$$

;Small signal

$$g_m = 2K_n (V_{GSQ} - V_{TN}) = 2\sqrt{K_n I_{DQ}}$$

$$r_o \cong \frac{1}{\lambda I_{DQ}}$$