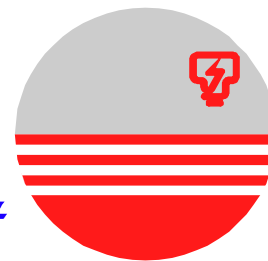


Name:
Student ID Number:
Section:
Lecturer: Dr Azni Wati/ Dr Fazrena Azlee/
Dr Jehana Ermy/ Dr Jamaludin
Table Number:

**UNIVERSITI
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College of Engineering
Department of Electronics and Communication Engineering

Test 2 – MODEL ANSWERS

SEMESTER 1, ACADEMIC YEAR 2015/2016

Subject Code : **EEEB273**
Course Title : **Electronics Analysis & Design II**
Date : **22 August 2015**
Time Allowed : **1 hour 45 minutes**

Instructions to the candidates:

1. Write your Name and Student ID number. Circle Lecturer for your section.
2. Write all your answers using pen. **DO NOT USE PENCIL** except for the diagram.
3. **ANSWER ALL QUESTIONS.**
4. **WRITE YOUR ANSWER ON THIS QUESTION PAPER.**

NOTE: DO NOT OPEN THE QUESTION PAPER UNTIL INSTRUCTED TO DO SO.



GOOD LUCK!



Question Number	Q1	Q2	Q3	Total
Marks				

Question 1 [40 marks]

- (a) The differential amplifier shown in **Figure 1** has a pair of pnp bipolars as input devices and a pair of npn bipolars connected as an active load. The circuit bias is $I_Q = 0.15 \text{ mA}$, and the transistor parameters are $\beta = 100$, and $V_A = 100 \text{ V}$.
- (i) **Draw** the active load circuit to complete the circuit in **Figure 1**. [6 marks]
 - (ii) **Find the open-circuit** differential-mode voltage gain, A_d . [8 marks]
 - (iii) **Calculate** the value of a load resistance R_L connected to the output v_O if the differential-mode voltage gain A_d is to be reduced to 524 V/V . [6 marks]

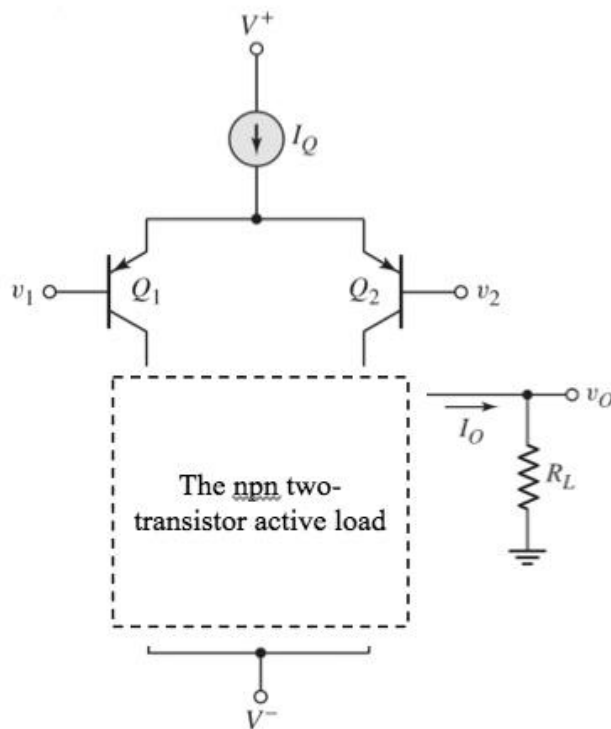


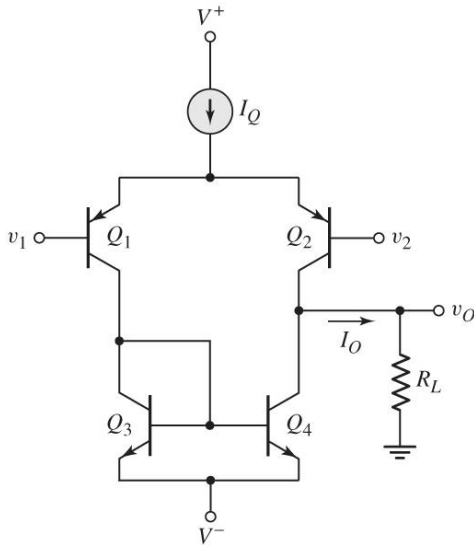
Figure 1

Answer for Question 1(a)(i)

Answer for Question 1(a)

Answer for Question 1(a)

Q1(a)(i)



3 marks: correct label
3 marks: correct placement

Q1(a)(ii)

$$r_{o2} = \frac{V_A}{I_{CQ2}} = \frac{V_A}{I_Q/2} = \frac{100}{0.15\text{m}/2} = 1.333\text{M}\Omega \quad [2]$$

$$r_{o4} = \frac{V_A}{I_{CQ4}} = \frac{V_A}{I_Q/2} = \frac{100}{0.15\text{m}/2} = 1.333\text{M}\Omega \quad [2]$$

$$g_{m2} = \frac{I_{CQ2}}{V_T} = \frac{I_Q}{2V_T} = \frac{0.15\text{m}}{2(0.026)} = 2.8845\text{mA/V} \quad [2]$$

$$A_d = g_{m2}(r_{o2} \parallel r_{o4}) = (2.8845\text{m})(1.333\text{M} \parallel 1.333\text{M}) = 1923 \quad [2]$$

Q1(a)(iii)

$$A_d = g_{m2}(r_{o2} \parallel r_{o4} \parallel R_L) \quad [2]$$

$$524 = (2.8845\text{m})(1.333\text{M} \parallel 1.333\text{M} \parallel R_L) \quad [2]$$

$$R_L = 250\text{k}\Omega \quad [2]$$

(b) For the differential amplifier with cascode active load in Figure 2 it is given that the circuit parameters are: $V^+ = 3\text{ V}$, $V^- = -3\text{ V}$, and $I_Q = 1\text{ mA}$. NMOS transistor parameters are: $V_{TN} = 0.7\text{ V}$, $k'_n = 130\ \mu\text{A}/\text{V}^2$, $(W/L)_n = 100$ and $\lambda_n = 0.1\text{ V}^{-1}$; and the PMOS transistor parameters are: $V_{TP} = -0.8\text{ V}$, $k'_p = 35\ \mu\text{A}/\text{V}^2$, $(W/L)_p = 200$ and $\lambda_p = 0.2\text{ V}^{-1}$.

- (i) Find the differential gain A_d . [8 marks]
- (ii) It is given that the common-mode gain, A_{cm} for the circuit is -0.002 . Calculate the common-mode rejection ratio, $CMRR$ in dB. [4 marks]
- (iii) It is given that the voltage across the constant current source I_Q , $V_{I_Q} = 0.6\text{ V}$. Figure 2 shows where the V_{I_Q} is. Calculate the maximum and minimum output voltage v_o . State any assumptions. [8 marks]

Answer for Question 1(b)

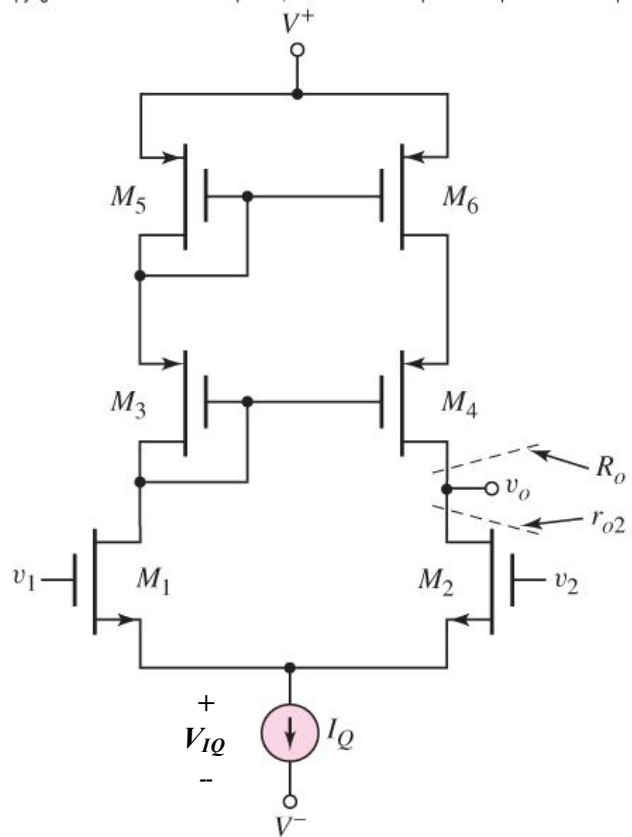


Figure 2

Answer for Question 1(b)

Q1(b)(i)

$$A_d = g_{m1}(r_{o2} \parallel R_o) \quad [1]$$

$$I_{D1} = I_Q / 2 = I_{D2} = I_{D3} = I_{D4} = I_{D5} = I_{D6} = 1mA / 2 = 0.5mA$$

$$g_{m1} = 2\sqrt{K_n I_{D1}} = 2\sqrt{\left(\frac{k'_n}{2}\right)\left(\frac{W}{L}\right)_1 I_{D1}} = 2\sqrt{\left(\frac{130}{2}\right)(100)(0.5m)} = 3.61mA/V \quad [1]$$

$$r_{o2} = \frac{1}{\lambda_n I_{D2}} = \frac{1}{(0.1)(0.5m)} = 20k\Omega \quad [1]$$

$$r_{o4} = \frac{1}{\lambda_p I_{D4}} = \frac{1}{(0.2)(0.5m)} = 10k\Omega = r_{o6} \quad [1]$$

$$g_{m4} = 2\sqrt{K_p I_{D4}} = 2\sqrt{\left(\frac{k'_p}{2}\right)\left(\frac{W}{L}\right)_4 I_{D4}} = 2\sqrt{\left(\frac{35}{2}\right)(200)(0.5m)} = 2.65mA/V \quad [1]$$

$$R_o = g_{m4} r_{o4} r_{o6} = (2.65m)(10k)(10k) = 265k\Omega \quad [2]$$

$$A_d = (3.61m)(20k \parallel 2.65k) = 67.1V/V \quad [1]$$

Q1(b) (ii)

$$CMRR = \left| \frac{A_d}{A_{cm}} \right| = \left| \frac{67.1}{-0.002} \right| = 33550 \quad [2]$$

$$CMRR_{dB} = 20\log|CMRR| = 20\log(33550) = 90.5dB \quad [2]$$

Q1(b)(iii)

$$V_o(\text{max}) = V^+ - V_{SD6}(\text{sat}) - V_{SD4}(\text{sat}) \quad [1]$$

$$V_{SG4} = V_{SG6} \Rightarrow I_{D4} = \left(\frac{k_p'}{2} \right) \left(\frac{W}{L} \right)_4 (V_{SG1} + V_{TP})^2$$

$$0.5m = \left(\frac{35}{2} \right) (200) (V_{SG4} + (-0.8))^2$$

$$\rightarrow V_{SG4} = 1.178V \quad [1]$$

$$V_{SD4}(\text{sat}) = V_{SG4} + V_{TP} = 1.178 + (-0.8) = 0.378V = V_{SD6}(\text{sat}) \quad [1]$$

$$V_o(\text{max}) = 3 - 2(0.378) = 2.24V \quad [1]$$

$$V_o(\text{min}) = V_{DS2}(\text{sat}) + V_{IQ} + V^- \quad [1]$$

$$V_{GS2} \Rightarrow I_{D2} = \left(\frac{k_n'}{2} \right) \left(\frac{W}{L} \right)_2 (V_{GS2} - V_{TN})^2$$

$$0.5m = \left(\frac{130}{2} \right) (100) (V_{GS1} - 0.7)^2$$

$$\rightarrow V_{GS1} = 0.977V \quad [1]$$

$$V_{DS2}(\text{sat}) = V_{GS2} - V_{TN} = 0.977 - 0.7 = 0.277V \quad [1]$$

$$V_o(\text{min}) = 0.277 + 0.6 + (-3) = -2.12V \quad [1]$$

Question 2 [30 marks]

The circuit in **Figure 3** shows a simple multi-stage BJT op-amp, consisting of three different stages. It is given that for all transistors: $\beta = 100$, $r_o = 500 \text{ k}\Omega$, $g_m = 5 \text{ mA/V}$, and $r_\pi = 3 \text{ k}\Omega$.

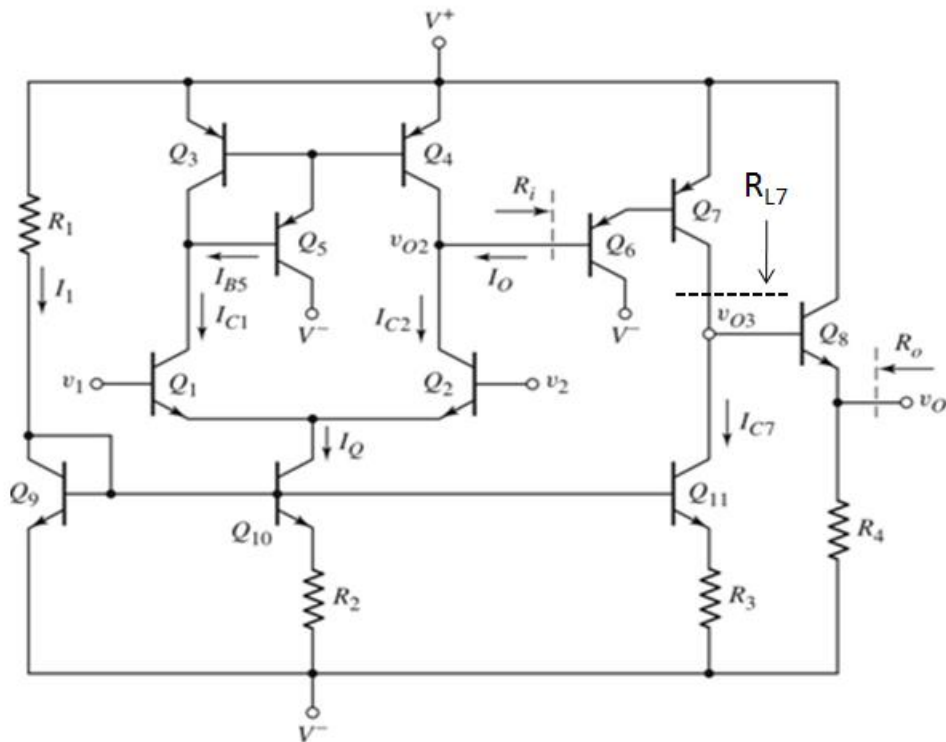


Figure 3

- (a) It is also given that $R_3 = 250 \Omega$ and $R_4 = 10 \text{ k}\Omega$. For Q_7 , the **Early voltage** V_A is assumed to be infinite. **Calculate the small signal input impedance** at the collector of Q_7 , i.e. R_{L7} as indicated in the **Figure 3**. [12 marks]

- (b) **Calculate** the small-signal voltage gain of the gain stage, $A_2 = V_{O3}/V_{O2}$. Given that:

$$V_{O3} = I_{c7} R_{L7}$$

$$V_{O2} = I_{b6} R_i$$

[10 marks]

- (c) **Determine** the output resistance of the amplifier, R_o .

[8 marks]

Answer for Question 2

Q2(a)

$$R_{c11} = r_{o11}(1 + g_{m11}R'_E) \quad [2]$$

$$R'_E = r_{\pi11} \parallel R_3 = 3k \parallel 250 = 230.8\Omega \quad [2]$$

$$R_{c11} = r_{o11}(1 + g_{m11}R'_E) = 500k(1 + (5m)(230.8)) = 1.077M\Omega \quad [2]$$

$$R_{b8} = r_{\pi8} + (1 + \beta)R_4 = 3k + (101)(10k) = 1.013M\Omega \quad [3]$$

$$R_{L7} = R_{c11} \parallel R_{b8} = 1.077M \parallel 1.013M = \mathbf{522\ k\Omega} \quad [3]$$

Q2(b)

$$V_{o3} = I_{c7}R_{L7} = (\beta I_{b7})R_{L7} = \beta(1 + \beta)I_{b6}R_{L7} \quad [3, 2]$$

$$A_v = \frac{V_{o3}}{V_{o2}} = \frac{\beta(1 + \beta)R_{L7}}{R_i}$$

$$R_i = r_{\pi6} + r_{\pi7}(1 + \beta) = 3k + (101)(3k) = 306k\Omega \quad [3]$$

$$A_v = \frac{V_{o3}}{V_{o2}} = \frac{100(101)522k}{306k} = 17229 \quad [2]$$

Q2(c)

$$R_o = R_4 \parallel \left(\frac{r_{\pi8} + Z}{(1 + \beta)} \right) \quad [3]$$

$$Z = R_{c11} \parallel R_{c7} = R_{c11} \quad [1]$$

$$R_{c7} = r_{o7} = \infty \quad [1]$$

$$R_{c11} = r_{o11}(1 + g_{m11}R'_E) = 1.077\text{ M}\Omega \quad [1]$$

$$R_o = 10k \parallel \left(\frac{3k + 1.077M}{(101)} \right) = 5.167k\Omega \quad [2]$$

Question 3 [30 marks]

A class-A emitter follower biased with a constant current source is shown in **Figure 4**. Assume circuit parameters of $V^+ = 12\text{ V}$, $V^- = -12\text{ V}$, and $R_L = 50\ \Omega$. The transistor parameters are $\beta = 40$, $V_{BE(\text{on})} = 0.7\text{ V}$, and $v_{CE(\text{sat})} = 0.7\text{ V}$. The minimum current in Q_1 is to be $i_{E1}(\text{min}) = 20\text{ mA}$.

- (a) **Determine** the value of R that will produce the maximum possible output voltage swing. **What** is the value of I_Q ? [12 marks]
- (b) For output voltage $v_O = 0$, **find** the power dissipated in the transistor Q_1 and the power dissipated in the transistor Q_2 . [6 marks]
- (c) **Determine** the power conversion efficiency (η) for a symmetrical sine-wave output voltage with a peak value of 10 V . [12 marks]

Answer for Question 3

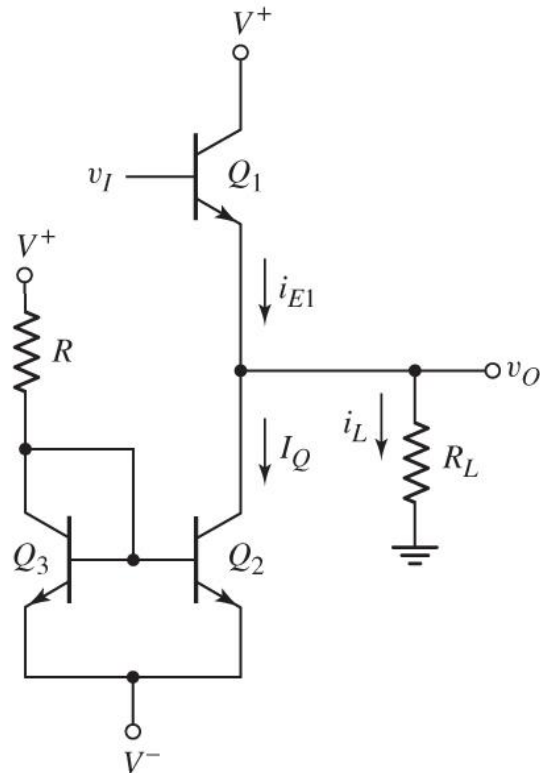


Figure 4

Answer for Question 3

Q3(a)

$$i_{E1} = I_Q + i_L$$

$$i_{E1}(\text{min}) = I_Q + i_L(\text{min}) \quad [2]$$

$$i_L(\text{min}) = \frac{v_o(\text{min})}{R_L} = \frac{V^- + v_{CE2}(\text{min})}{R_L} = \frac{-12 + 0.7}{50} = -226\text{mA} \quad [2]$$

$$I_Q = i_{E1}(\text{min}) - i_L(\text{min}) = 20\text{mA} - (-226\text{mA}) = 246\text{mA} \quad [2]$$

$$I_R = I_Q(1 + 2/\beta) \quad [2]$$

$$I_R = (246\text{mA})(1 + 2/40) = 258.3\text{mA} \quad [1]$$

$$R = \frac{V^+ - V_{BE3}(\text{on}) - V^-}{I_R} \quad [2]$$

$$R = \frac{12 - 0.7 - (-12)}{258.3\text{mA}} = \frac{23.3\text{V}}{258.3\text{mA}} = 90.205 \Omega [1]$$

Q3(b)

$$P_{DQ1} = V_{CE1} I_{C1} = V_{CE1} I_{E1} = (V^+ - v_o)(I_Q + i_L) = (12 - 0)(246\text{mA} + 0) = 2.952\text{W} \quad [3]$$

$$P_{DQ2} = V_{CE2} I_{C2} = (v_o - V^-)(I_Q + i_L) = (0 - (-12))(246\text{mA} + 0) = 2.952\text{W} \quad [3]$$

Q3(c)

$$\eta = \frac{\overline{P}_L}{\overline{P}_S} \times 100\% = [3]$$

$$\overline{P}_L = \frac{[v_P]^2}{2R_L} = \frac{10 \times 10}{2 \times 50} = 1\text{W} \quad [3]$$

\overline{P}_S is calculated using power dissipated in Q1 and Q2:

$$\overline{P}_S = P_{DQ1} + P_{DQ2} = (V^+ - V^-)I_Q = (12 - (-12))(246\text{mA}) = 5.904\text{W} \quad [3]$$

$$\eta = \frac{1\text{W}}{5.904\text{W}} \times 100\% = 16.937\% \quad [3]$$

OR \overline{P}_S is calculated using power dissipated in ALL transistors and R:

$$\overline{P}_S = P_{DQ1} + P_{DQ2} + P_{DQ3R} = (V^+ - V^-)(I_Q + I_R) = (12 - (-12))(246\text{mA} + 258.3\text{mA}) = 12.1032\text{W} \quad [3]$$

$$\eta = \frac{1\text{W}}{12.103\text{W}} \times 100\% = 8.262\% \quad [3]$$

BASIC FORMULA FOR TRANSISTOR

BJT

$$i_C = I_S e^{v_{BE}/V_T}; \text{npn}$$

$$i_C = I_S e^{v_{EB}/V_T}; \text{pnp}$$

$$i_C = \alpha i_E = \beta i_B$$

$$i_E = i_B + i_C$$

$$\alpha = \frac{\beta}{\beta + 1}$$

; Small signal

$$\beta = g_m r_\pi$$

$$g_m = \frac{I_{CQ}}{V_T}$$

$$r_\pi = \frac{\beta V_T}{I_{CQ}}$$

$$r_o = \frac{V_A}{I_{CQ}}$$

$$V_T = 26 \text{ mV}$$

MOSFET

; N – MOSFET

$$v_{DS}(\text{sat}) = v_{GS} - V_{TN}$$

$$i_D = K_n [v_{GS} - V_{TN}]^2$$

$$K_n = \frac{k'_n}{2} \cdot \frac{W}{L}$$

; P – MOSFET

$$v_{SD}(\text{sat}) = v_{SG} + V_{TP}$$

$$i_D = K_p [v_{SG} + V_{TP}]^2$$

$$K_p = \frac{k'_p}{2} \cdot \frac{W}{L}$$

; Small signal

$$g_m = 2\sqrt{K_n I_{DQ}}$$

$$r_o \cong \frac{1}{\lambda I_{DQ}}$$