Name:

Student ID Number:

Section:

Lecturer: Dr Azni Wati/ Dr Jehana Ermy/

Dr Jamaludin

Table Number:



# College of Engineering

Department of Electronics and Communication Engineering

# Test 2

### **SEMESTER 2, ACADEMIC YEAR 2015/2016**

Subject Code	:	<b>EEEB273</b>
Course Title	:	Electronics Analysis & Design II
Date	:	9 January 2016
Time Allowed	:	1 hour 45 minutes

### **Instructions to the candidates:**

- 1. Write your Name and Student ID number. Circle Lecturer for your section.
- 2. Write all your answers using pen. DO NOT USE PENCIL except for the diagram.
- 3. ANSWER ALL QUESTIONS.
- 4. WRITE YOUR ANSWER ON THIS QUESTION PAPER.

NOTE: DO NOT OPEN THE QUESTION PAPER UNTIL INSTRUCTED TO DO SO.



Question Number	Q1	Q2	Q3	Total
Marks				

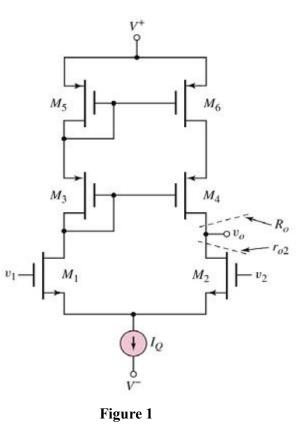
#### **<u>Question 1</u>** [40 marks]

Figure 1 shows a MOSFET differential amplifier with active load circuit biased with constant current source  $I_Q$ . It is given that  $V^+ = 10$  V, V = -10 V, and  $I_Q = 0.23$  mA.

Also, the NMOS transistor parameters are:  $V_{TN} = 1 \text{ V}$ ,  $k'_n = 100 \text{ }\mu\text{A/V}^2$  and  $\lambda_n = 0.015 \text{ V}^{-1}$ , and the PMOS transistor parameters are:  $V_{TP} = -1 \text{ V}$ ,  $k'_p = 80 \text{ }\mu\text{A/V}^2$  and  $\lambda_p = 0.01 \text{ V}^{-1}$ . Given that the transistorsø aspect ratios  $(W/L)_{1-2} = 5$  and  $(W/L)_{3-6} = 10$ .

- (a) State the function of each transistor  $M_1$  to  $M_6$  in the Figure 1. [6 marks]
- (b) **Determine** the maximum **common-mode voltage input**,  $v_{cm}(max)$ , that can be applied such that the transistors are still biased in saturation region. [8 marks]
- (c) Draw the ac equivalent circuit for the differential-mode input  $(v_1 = +v_d/2 \text{ and } v_2 = v_d/2)$ . Indicate the resultant ac currents in all transistors. [6 marks]
- (d) **Determine** the output resistance *Ro* in the Figure 1. [8 marks]
- (e) **Calculate** the differential-mode voltage gain  $(A_d)$  of the diff-amp. [8 marks]
- (f) **Comment** how the output resistance of the diff-amp can be changed. [4 marks]

#### **Answers for Question 1**



Answer for Question 1 (Cont.)

Answer for Question 1 (Cont.)

#### Answers:

#### **<u>Question 2</u>** [30 marks]

The circuit in Figure 2 shows a Darlington pair emitter-follower configuration. Assume  $\beta = 120$  for all NPN transistors and  $\beta = 90$  for all PNP transistors. Let  $V_{A7} = 60$  V for  $Q_7$ ,  $V_{A11} = 120$  V for  $Q_{11}$ , and  $V_A = \infty$  for all other transistors.

Given that  $R_3 = 200 \Omega$ ,  $R_4 = 5 k\Omega$ ,  $I_{C7} = I_{C11} = 0.25 mA$ , and  $I_{C8} = 1 mA$ .

- (a) **Calculate** the value of  $R_i$  of the circuit in the Figure 2. [10 marks]
- (b) Find the value of *R*<sub>0</sub> of the circuit in the Figure 2.

[20 marks]

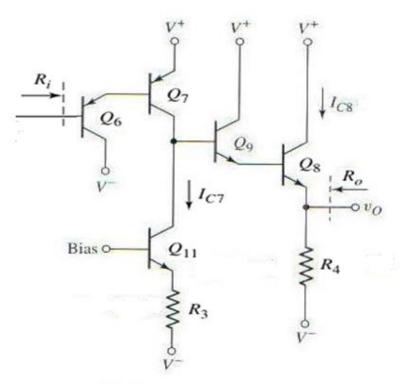


Figure 2

Answer for Question 2

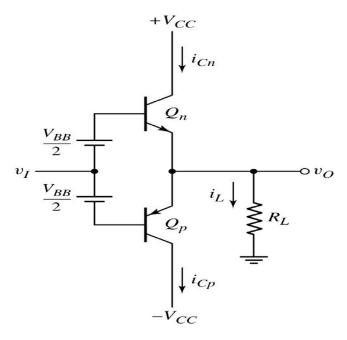
Answer for Question 2 (Cont.)

#### **<u>Question 3</u>** [30 marks]

Figure 3 shows a simplified class-AB output stage with BJTs. The circuit parameters are  $V_{CC} = 5$ Volts and  $R_L = 1 \text{ k}\Omega$ . The saturation current is  $I_S = 2 \times 10^{-15} \text{ A}$ .

- (a) When  $v_I = 0$ , calculate the value for  $V_{BB}$  that gives  $i_{Cn} = i_{Cp} = 1$  mA. [6 marks]
- (b) Find the power dissipated in transistors  $Q_n$  and  $Q_p$  when  $v_I = 0$ . [3 marks]
- (c) **Determine**  $i_L$ ,  $i_{Cn}$ ,  $i_{Cp}$ , and  $v_I$  if  $v_0 = -3.5$  V. [12 marks]
- (d) Based on answers in **part (c)**, **calculate** the power dissipated in  $Q_n$ ,  $Q_p$ , and  $R_L$ . [9 marks]

#### **Answer for Question 3**





Answer for Question 3 (Cont.)

# **BASIC FORMULA FOR TRANSISTOR**

## <u>BJT</u>

$$i_{C} = I_{S} e^{v_{BE}/V_{T}}; \text{npn}$$
$$i_{C} = I_{S} e^{v_{EB}/V_{T}}; \text{pnp}$$
$$i_{C} = \alpha i_{E} = \beta i_{B}$$
$$i_{E} = i_{B} + i_{C}$$
$$\alpha = \frac{\beta}{\beta + 1}$$

;Small signal

$$\beta = g_m r_{\pi}$$
$$g_m = \frac{I_{CQ}}{V_T}$$
$$r_{\pi} = \frac{\beta V_T}{I_{CQ}}$$
$$r_o = \frac{V_A}{I_{CQ}}$$
$$V_T = 26 \text{ mV}$$

## **MOSFET**

; N – MOSFET  

$$v_{DS}$$
 (sat) =  $v_{GS} - V_{TN}$   
 $i_D = K_n [v_{GS} - V_{TN}]^2$   
 $K_n = \frac{k'_n}{2} \cdot \frac{W}{L}$ 

; P – MOSFET  $v_{SD}(\text{sat}) = v_{SG} + V_{TP}$   $i_D = K_p [v_{SG} + V_{TP}]^2$  $K_p = \frac{k'_p}{2} \cdot \frac{W}{L}$ 

;Small signal  $g_m = 2\sqrt{K_{?}I_{DQ}}$  $r_o \cong \frac{1}{\lambda I_{DQ}}$