



**COLLEGE OF ENGINEERING  
PUTRAJAYA CAMPUS  
FINAL EXAMINATION  
**SOLUTION**  
SEMESTER 1 2016 / 2017**

PROGRAMME : Bachelor of Electrical & Electronics Engineering (Honours)  
Bachelor of Electrical Power Engineering (Honours)

SUBJECT CODE : EEEB273

SUBJECT : ELECTRONIC ANALYSIS AND DESIGN II

DATE : September 2016

TIME : 3 Hours

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**INSTRUCTIONS TO CANDIDATES:**

1. This paper contains **FIVE** (5) questions in **EIGHT** (8) pages.
2. Answer **ALL** questions.
3. Write **all** answers in the answer booklet provided. Use **pen** to write your answer.
4. Write answer to different question on a **new page**.
5. For all calculations, assume that  $V_T = 26 \text{ mV}$ .

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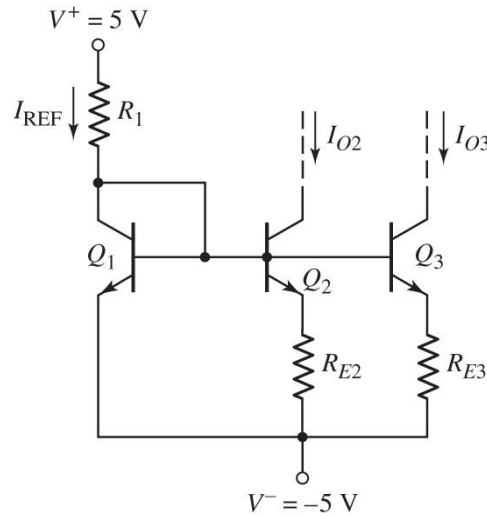
***THIS QUESTION PAPER CONSISTS OF EIGHT (8) PRINTED PAGES INCLUDING THIS COVER PAGE.***

**QUESTION 1 [20 MARKS]**

(a) Consider the Widlar current-source circuit with multiple output shown in **Figure 1**. Assume that  $V_{BE1(\text{on})} = 0.7 \text{ V}$ . The circuit parameters are  $R_1 = 10 \text{ k}\Omega$ ,  $R_{E2} = 1 \text{ k}\Omega$ , and  $R_{E3} = 2 \text{ k}\Omega$ .

Calculate  $I_{REF}$ ,  $I_{O2}$ , and  $I_{O3}$ .

[10 marks]



**Figure 1**

Answers:

Using KVL rule,  $I_{REF} = \frac{V^+ - V_{BE1} - V^-}{R_1} = \frac{5 - 0.7 - 5}{10k} = \underline{\underline{0.9300 \text{ mA}}}$  [2, 1, 1 marks]

Solving for Widlar CS,

$I_{O2} R_{E2} = V_T \ln \left( \frac{I_{REF}}{I_{O2}} \right)$  [2 marks]

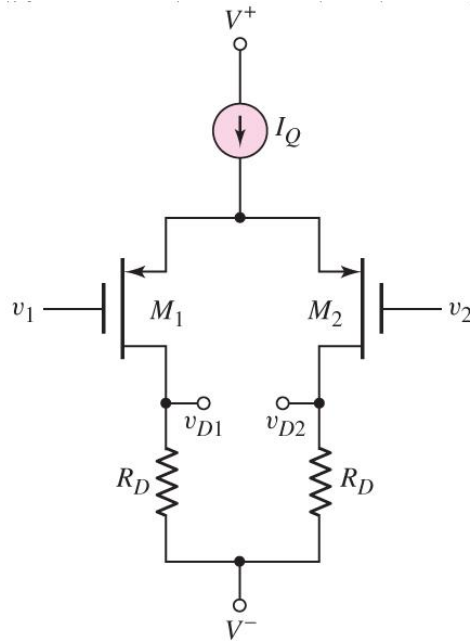
$I_{O2} R_{E2} = V_T \ln \left( \frac{I_{REF}}{I_{O2}} \right) \rightarrow I_{O2}(1k) = (0.026) \ln \left( \frac{0.9300\text{mA}}{I_{O2}} \right)$

$I_{O2} \cong \underline{\underline{68 \mu\text{A}}}$  [2 marks]

$I_{O3} R_{E3} = V_T \ln \left( \frac{I_{REF}}{I_{O3}} \right) \rightarrow I_{O3}(2k) = (0.026) \ln \left( \frac{0.9300\text{mA}}{I_{O3}} \right)$

$I_{O3} \cong \underline{\underline{40.7 \mu\text{A}}}$  [2 marks]

- (b) The circuit shown in **Figure 2** has circuit and transistor parameters as  $V^+ = +3 \text{ V}$ ,  $V^- = -3 \text{ V}$ ,  $R_D = 360 \text{ k}\Omega$ ,  $V_{TP} = -0.4 \text{ V}$ ,  $K_p = 30 \mu\text{A}/\text{V}^2$ , and  $\lambda = 0$ . The bias current is given as  $I_Q = 12 \mu\text{A}$ . Calculate voltage  $V_{SD1}$  for  $v_1 = v_2 = 0$ . **[10 marks]**



**Figure 2**

Answers:

As  $v_1 = v_2 = 0$ ,

$$I_D = K_p(V_{SG} + V_{TP})^2 \quad [1 \text{ mark}]$$

$$I_D = I_Q/2 = 12\mu/2 = \underline{6 \mu\text{A}} \quad [2 \text{ marks}]$$

$$V_{SG} = \sqrt{\frac{I_D}{K_p}} - V_{TP} \rightarrow \sqrt{\frac{6\mu}{30}} + 0.4 = \underline{0.8470 \text{ V}} \quad [2 \text{ marks}]$$

$$V_S = \underline{0.8470 \text{ V}} \quad [1 \text{ mark}]$$

$$V_D = I_D R_D + V^- = (6\mu)(360\text{k}) + (-3) = \underline{-0.8400 \text{ V}} \quad [2 \text{ marks}]$$

$$\text{So, the } Q\text{-point is } V_{SD} = V_S - V_D = 0.8470 - (-0.8400) = \underline{1.690 \text{ V}} \quad [2 \text{ marks}]$$

**QUESTION 2 [20 MARKS]**

(a) The differential amplifier shown in **Figure 3** is biased by a **0.20 mA** constant current source (i.e.  $I_Q = 0.20 \text{ mA}$ ). It is to be redesigned to use an active load in order to increase its differential-mode voltage gain ( $A_d$ ). The active load to be used is a **Current Mirror** using **PMOS transistors** to replace the resistors ( $R_D$ ) in the differential amplifier. Let supply voltages be  $\pm 5\text{V}$ .

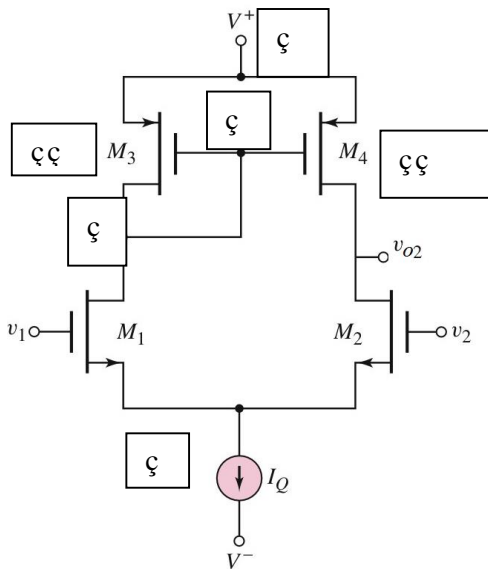
Assume that NMOS devices are available with the following parameters:  $K_n = 400 \mu\text{A/V}^2$ ,  $V_{TN} = 0.5 \text{ V}$ , and  $\lambda_n = 0.02 \text{ V}^{-1}$

Assume that PMOS devices are available with the following parameters:  $K_p = 200 \mu\text{A/V}^2$ ,  $V_{TP} = -1 \text{ V}$ , and  $\lambda_p = 0.02 \text{ V}^{-1}$

- (i) **Draw the new circuit** incorporating the **active load's full circuit diagram**. Label the circuit correctly and clearly with appropriate symbols and numbering for transistors used in circuit. Leave  $I_Q$  symbol as it is in **Figure 3**. [4 marks]
- (ii) Determine the **differential-mode voltage gain** ( $A_d$ ) of the circuit. [6 marks]

**Question 2a**

(i)

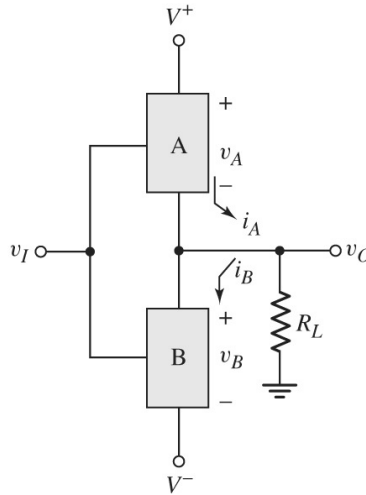


$\zeta = 0.5 \text{ mark}$   
Total [4]

- (ii)  $v_{O2} = g_{m2} v_d (r_{O2} \parallel r_{O4})$  [1 mark]
- $A_d = v_{O2} / v_d = g_{m2} (r_{O2} \parallel r_{O4})$  [1 mark]
- $g_{m2} = 2\sqrt{(K_n I_Q / 2)} = 2\sqrt{[(400\mu)(0.2\text{m}/2)]} = 0.4 \text{ mA/V}$  [1.5 marks]
- $r_{O2} = 1/(\lambda_n I_Q / 2) = 1/ [(0.02)( 0.2\text{m}/ 2)] = 500 \text{ k}\Omega$  [1 mark]
- $r_{O4} = 1/(\lambda_p I_Q / 2) = 1/ [(0.02)( 0.2\text{m}/ 2)] = 500 \text{ k}\Omega$  [0.5 mark]
- $r_{O2} \parallel r_{O4} = 250 \text{ k}$  [0.5 mark]
- $A_d = (0.4\text{m})(250\text{k}) = 100$  [0.5 mark]

(b) Consider an **idealized class-B** output stage as shown in **Figure 4**. The output stage is to deliver **50 W of average power to the load** at a **maximum output voltage of 11.3 V**. Let the power supply voltages be **±12 volts**. The average current supplied by the supply units can be calculated by using  $I_{av} = I_p / \pi$ .

- (i) Calculate the **peak output current,  $I_p$** . **[4 marks]**
- (ii) Calculate the **total average power supplied** by the supply units **[4 marks]**
- (iii) Calculate the **power conversion efficiency** for this circuit. **[2 marks]**



**Figure 4**

**Question 2b**

$$P_L = V_p I_p / 2 = 50 \quad [2]$$

$$I_p = 2 P_L / V_p = 2(50) / 11.3 = 8.85 \text{ A} \quad [2]$$

$$I_{ave} = I_p / \pi = 8.85 / \pi = 2.817 \text{ A} \quad [2]$$

$$P_{S(ave)} = 2V_{CC} I_{ave} = 2(12)(2.817) = 67.61 \text{ W} \quad [2]$$

$$\eta = P_L / P_{S(ave)} = (50 / 67.61) \times 100 = 73.95\% \quad [2]$$

**QUESTION 3 [20 MARKS]**

Figure 5 shows a multistage amplifier circuit with transistor parameters of  $\beta = 120$  and  $V_A = \infty$ ,  $V_{BE(on)} = V_{EB(on)} = 0.7V$ . It is given that  $V^+ = 10 V$ .

- (a) Explain the functions of transistors  $Q_1$ ,  $Q_2$  and  $Q_3$  in the multistage amplifier. [5 marks]
- (b) The circuit is such that **zero dc output voltage** is established. Calculate the value of resistors  $R_{C2}$  and  $R_{C3}$  if currents  $I_Q = 0.5 \text{ mA}$  and  $I_{C3} = 1 \text{ mA}$ . [10 marks]
- (c) **Determine** the output resistance,  $R_o$ . [5 marks]

**Question 3(a)**

Q1 & Q2 are Darlington Pair, [1 mark]  
 provides large gain [0.5 mark] and large input resistance [0.5 mark]

Q3 is an emitter follower / common collector amplifier. [1 mark]

The gain is unity [0.5 mark] and has low output resistance [0.5 mark].

It acts as buffer / provides impedance matching to the load. [1 mark]

**Question 3(b)**

For  $V_o = V_{E3} = 0V$ :  
 $I_{C3} = (V^+ - V_o) / R_{C3}$  eqn 1 [2 marks]

So  $R_{C3} = (V^+ - 0) / I_{C3} = 10/1\text{mA} = 10 / 1\text{m} = \mathbf{10 \text{ k}\Omega}$  [2 marks]

$I_Q = (V^+ - V_{C2})/R_{C2}$  eqn 2 [2 marks]  
 $V_{C2} = V_{B3}$ ,  $V_{B3} = V_{E3} \hat{=} V_{EB3}$  eqn 3 [2 marks]  
 $V_{B3} = V_{E3} \hat{=} V_{EB3} = 0 \hat{=} 0.7V = -0.7V = V_{C2}$  [1 mark]  
 $I_Q = (V^+ - V_{C2})/R_{C2} = 10 \hat{=} (-0.7) / R_{C2} = 10.7/R_{C2}$

So  $R_{C2} = 10.7V / I_Q = 10.7 / 0.5\text{m} = \mathbf{21.4 \text{ k}\Omega}$  [1 mark]

**Question 3(c)**

$R_o = R_{C3} \parallel \frac{r_{\pi 3} + [R_{C2} \parallel r_{o2}]}{1 + \beta}$  [2 marks]

$r_{\pi 3} = V_T / I_{C3} = 26\text{m} / 1\text{m} = \mathbf{3.12 \text{ k}\Omega}$  [1 mark]  
 $r_{o2} = V_A / I_{C2} = V_A / I_Q = \hat{\infty} / 0.5\text{m} = \infty$  [1 mark]  
 $R_{C2} \parallel r_{o2} = R_{C2}$

$R_o = 10\text{k} \parallel [ 3.12\text{k} + 21.4\text{k} ] / (1 + 120) = \mathbf{198.6 \Omega}$  [1 mark]

**QUESTION 4 [20 MARKS]**

Consider a **standard 741 operational amplifier** (op-amp) circuit as shown in **Figure 6a**. Study **Figure 6a** carefully and observe labelling and values for the resistors in the circuit. Load resistance  $R_L = 2 \text{ k}\Omega$  is connected to the Output of the 741 op-amp. The op-amp is supplied by  $\pm 15 \text{ V DC}$  voltages.

The transistors have  $\beta_n = 200$ ,  $\beta_p = 50$ , **Early voltages**  $V_{AN} = V_{AP} = 50 \text{ V}$ ,  $V_{BE(\text{on})} = V_{EB(\text{on})} = 0.6 \text{ V}$ , and the reverse saturation current  $I_S = 5 \times 10^{-16} \text{ A}$ .

From **DC analysis**, bias currents for selected transistors are  $I_{C13A} = 0.18 \text{ mA}$ ,  $I_{C13B} = 0.54 \text{ mA}$ ,  $I_{C16} = 15.8 \mu\text{A}$ ,  $I_{C17} = 0.54 \text{ mA}$ ,  $I_{C20} = 0.138 \text{ mA}$ , and  $I_{C22} = 0.18 \text{ mA}$ .

**Figure 6b** shows the AC equivalent circuit for the gain stage of the 741 op-amp. **Figure 6c** shows the AC equivalent circuit for the output stage of the 741 op-amp, which is used to calculate  $R_{i3}$  in the **Figure 6b**.

With small-signal analysis, the voltage gain for the gain stage ( $A_{v2}$ ) of the 741 op-amp can be calculated using the following formula:

$$A_{v2} = \frac{v_{o2}}{v_{o1}} = \frac{-\beta_n (1 + \beta_n) R_9 (R_{act2} \parallel R_{i3} \parallel R_{o17})}{R_{i2} (R_9 + R_{b17})}$$

$$R_{act2} = r_{o13B}$$

Where:  $R_{i3} = r_{\pi22} + (1 + \beta_p) [R_{19} \parallel R_{20}]$

$$R_{19} \cong R_{13A}$$

$$R_{20} = r_{\pi20} + (1 + \beta_p) R_L$$

$$R_{b17} = r_{\pi17} + (1 + \beta_n) R_8$$

**Calculate** the voltage gain for the gain stage ( $A_{v2}$ ) of the 741 op-amp if  $R_8$  is **short circuit**. Neglect base current in your calculations. Apply appropriate assumptions and recall standard formula for parameters which are not given above. **[20 marks]**

**Question 4**

$$R_{i2} = r_{\pi16} + (1 + \beta_n)R'_E \quad [1]$$

$$R'_E = R_9 \parallel [r_{\pi17} + (1 + \beta_n)R_8] = R_9 \parallel R_{b17} \quad [1]$$

$$r_{\pi16} = \frac{\beta_n V_T}{I_{C16}} = \frac{(200)(0.026)}{15.8} = 329 \text{ k}\Omega \quad [1]$$

$$r_{\pi17} = \frac{\beta_n V_T}{I_{C17}} = \frac{(200)(0.026)}{0.54\text{m}} = 9.63 \text{ k}\Omega \quad [1]$$

$$R_{b17} = r_{\pi17} + (1 + \beta_n)R_8 = 9.63\text{k} + (1 + 200)(0) = 9.63 \text{ k}\Omega \quad [1]$$

$$\Rightarrow R'_E = 50\text{k} \parallel 9.63\text{k} = 8.075 \text{ k}\Omega \quad [1]$$

$$\Rightarrow R_{i2} = 329\text{k} + (201)(8.075\text{k}) = 1.95 \text{ M}\Omega \quad [1]$$

$$R_{i3} = r_{\pi22} + (1 + \beta_p)[R_{19} \parallel R_{20}]$$

$$r_{\pi22} = \frac{\beta_p V_T}{I_{C13A}} = \frac{(50)(0.026)}{0.18\text{m}} = 7.22 \text{ k}\Omega \quad [1, 1]$$

$$R_{19} \cong R_{13A} = r_{o13A} = \frac{V_A}{I_{C13A}} = \frac{50}{0.18\text{m}} = 278 \text{ k}\Omega \quad [1]$$

$$r_{\pi20} = \frac{\beta_p V_T}{I_{C20}} = \frac{(50)(0.026)}{0.138\text{m}} = 9.42 \text{ k}\Omega \quad [1]$$

$$R_{20} = r_{\pi20} + (1 + \beta_p)R_L$$

$$R_{20} = 9.42\text{k} + (51)(2\text{k}) \cong 111 \text{ k}\Omega \quad [1]$$

$$\Rightarrow R_{i3} = 7.22\text{k} + (51)[278\text{k} \parallel 111\text{k}] = 4.05 \text{ M}\Omega \quad [1, 1]$$

$$R_{o17} = r_{o17}(1 + g_{m17}(r_{\pi17} \parallel R_8)); R_8 = 0 \quad [1]$$

$$\Rightarrow R_{o17} = r_{o17} = \frac{V_A}{I_{C17}} = \frac{50}{0.54\text{m}} = 92.6 \text{ k}\Omega \quad [1]$$

$$R_{act2} = r_{o13B} = \frac{V_A}{I_{C13B}} = \frac{50}{0.54\text{m}} = 92.6 \text{ k}\Omega \quad [1]$$

$$A_{v2} = \frac{-\beta_n(1 + \beta_n)R_9(R_{act2} \parallel R_{i3} \parallel R_{o17})}{R_{i2}(R_9 + R_{b17})}$$

$$A_{v2} = \frac{-(200)(201)(50\text{k})(92.6\text{k} \parallel 4.05\text{M} \parallel 92.6\text{k})}{1.95\text{M}(50\text{k} + 9.63\text{k})} \quad [2]$$

$$\Rightarrow A_{v2} = -792 \text{ V/V} \quad [1]$$



**QUESTION 5 [20 MARKS]**

(a) List down **two characteristics of an ideal op amp.** **[4 marks]**

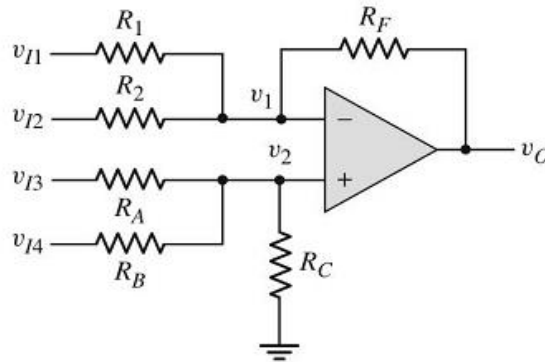
(b) State **three applications** for ideal op amp. **[3 marks]**

(c) Refer to the **generalised summing amplifier** using ideal op amp in **Figure 7**. The output voltage is given by:

$$v_O = -\frac{R_F}{R_1}v_{I1} - \frac{R_F}{R_2}v_{I2} + \left(1 + \frac{R_F}{R_N}\right)\left[\frac{R_P}{R_A}v_{I3} + \frac{R_P}{R_B}v_{I4}\right]$$

Design the summing amplifier for  $v_O = 2v_{I1} - 10v_{I2} + 3v_{I3} - v_{I4}$   
Use 500 k for the largest resistor value.

**[13 marks]**



**Figure 7**

**-END OF QUESTION PAPER-**

**Question 5 (a)**

$A_{od}$ : Internal differential gain (open loop gain) is considered to be  $\hat{O}$

$(v_2 \text{ ó } v_1)$ : Differential input voltage is assumed to be 0. If  $A_{od} = \hat{O}$  and  $v_O$  is finite, then  $v_2 \text{ é } v_1$

$R_i$ : Effective input resistance is assumed to be  $\hat{O}$ , so input currents  $i_1$  and  $i_2$  are essentially 0

$R_o$ : Effective output resistance is assumed to be 0, so output voltage is independent of any load connected to the output.

CMRR: Common mode rejection ratio =  $\hat{O}$

2 x 2 = [4 marks]

**Question 5 (b)**

Voltage to current converter, current to voltage converter, summing amplifier, instrumentation amplifier, difference amplifier, integrator and differentiator

3 x 1 = [3 marks]

**Question 5 (c) [13 marks]**

Rearrange and using  $v_O = -10v_{I1} - v_{I2} + 2v_{I3} + 3v_{I4}$

$$-R_F/R_1 = -10 \quad [1]$$

$$-R_F/R_2 = -1 \quad [1]$$

$$(1 + R_F/R_N)(R_P/R_A) = 2 \quad [1]$$

$$(1 + R_F/R_N)(R_P/R_B) = 3 \quad [1]$$

$$R_F = 10R_1 = R_2$$

$$\text{Let } R_F = \underline{500\text{k}\Omega} = R_2 \quad [1], [1]$$

$$\text{So } \underline{R_1 = 50\text{k}\Omega} \quad [1]$$

$$R_N = R_1 \parallel R_2 = 500\text{k} \parallel 50\text{k} = 45.5\text{k} \quad [1.5]$$

$$\text{So } (1 + R_F/R_N) = (1 + 500\text{k}/45.5\text{k}) = 12$$

$$\text{Thus } 12(R_P/R_A) = 2 \text{ and } 12(R_P/R_B) = 3$$

$$\text{So } 2R_A = 3R_B \text{ i.e. } R_A/R_B = 3/2$$

$$\text{Let } \underline{R_A = 500\text{k}\Omega}, \text{ then } \underline{R_B = 333\text{k}\Omega} \quad [1], [1]$$

$$R_P = R_A \parallel R_B \parallel R_C$$

$$R_A \parallel R_B = 500\text{k} \parallel 333\text{k} = 199.98\text{k} = 200\text{k}$$

$$\text{From } 12(R_P/R_A) = 2$$

$$R_P = 2R_A/12 = 2(500\text{k})/12 = 83.33\text{k} \quad [1.5]$$

$$\text{So } 83.3\text{k} = 200\text{k} \parallel R_C$$

$$\text{So } \underline{R_C = 142.9\text{k}\Omega} \quad [1]$$