

**COLLEGE OF ENGINEERING
PUTRAJAYA CAMPUS
FINAL EXAMINATION**

SEMESTER 1 2018 / 2019

MODEL ANSWERS

PROGRAMME	: Bachelor of Electrical & Electronics Engineering (Honours) Bachelor of Electrical Power Engineering (Honours)
SUBJECT CODE	: EEEB273
SUBJECT	: ELECTRONIC ANALYSIS AND DESIGN II
DATE	: September 2018
TIME	: 3 hours

INSTRUCTIONS TO CANDIDATES:

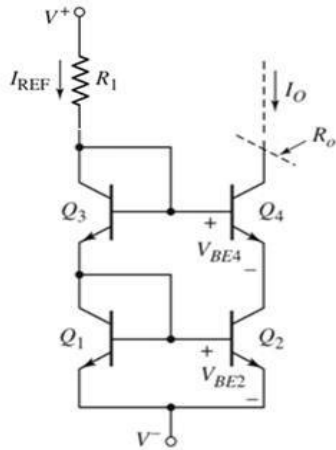
1. This paper contains **FIVE (5)** questions in **NINE (9)** pages.
2. Answer **ALL** questions.
3. Write **all** answers in the answer booklet provided. Use **pen** to write your answer.
4. Write answer to different question on a **new page**.

THIS QUESTION PAPER CONSISTS OF **NINE (9)** PRINTED PAGES INCLUDING THIS COVER PAGE.

Question 1 [20 marks]

Answers:

(a) [Each component carries 0.5 marks, total 4 marks]



(b)

$$I_{C2} = \beta I_{B2} = I_{E4} = \beta I_{B1}$$

$$I_{C4} = \alpha I_{E4} = \left(\frac{\beta}{\beta+1}\right)(\beta I_{B1}) = I_O \quad \rightarrow I_{B1} = \left(\frac{\beta+1}{\beta^2}\right)I_O$$

$$I_{B4} = \frac{I_{E4}}{\beta+1} = \left(\frac{1}{\beta+1}\right)(\beta I_{B1})$$

$$I_{C1} = \beta I_{B1} \text{ and } I_{E3} = (\beta + 2) I_{B1}$$

$$I_{B3} = \left(\frac{1}{\beta+1}\right)I_{E3} = \frac{1}{(\beta+1)}(\beta + 2)I_{B1} \text{ and } I_{C3} = \beta I_{B3} = \left(\frac{\beta}{\beta+1}\right)(\beta + 2) I_{B1}$$

$$I_{REF} = I_{C3} + I_{B3} + I_{B4}$$

$$\rightarrow I_{REF} = \left(\frac{\beta}{\beta+1}\right)(\beta + 2) I_{B1} + \frac{1}{(\beta+1)}(\beta + 2)I_{B1} + \left(\frac{1}{\beta+1}\right)(\beta I_{B1})$$

$$I_{REF} = \left[\frac{\beta^2+2\beta+\beta+2+\beta}{\beta+1}\right] I_{B1}$$

$$I_{REF} = \left[\frac{\beta^2+2\beta+\beta+2+\beta}{\beta+1}\right] \left[\left(\frac{\beta+1}{\beta^2}\right)I_O\right]$$

$$\rightarrow I_O = [I_{REF} / \left[1 + \frac{4}{\beta} + \frac{2}{\beta^2}\right]] \approx I_{REF} / \left[1 + \frac{4}{\beta}\right]$$

[Each carries 0.5 marks, total 5 marks]

c) $\beta = 150$, Since β is higher than 100, \therefore Approximation of $I_O = I_{REF}$ [1 mark]

$$I_{REF} = \frac{V^+ - V_{BE1} - V_{BE3} - V^-}{R_1} = \frac{5 - 0.7 - 0.7 - (-5)}{6 \times 10^3} = 1.433 \text{mA} \quad [2 \text{ marks}]$$

$$I_O = I_{REF} = 1.433 \text{mA} \quad [0.5 \text{ mark}]$$

$$R_O = \beta r_o = \beta \left(\frac{V_A}{I_O}\right) = 150 \left(\frac{100}{1.433 \text{mA}}\right) = 10.465 \text{M}\Omega \quad [3.5 \text{ marks}]$$

d) $g_{m4} = \frac{I_O}{V_T}$ [1 mark]

$$g_{m4} = \frac{1.433 \text{mA}}{26 \text{mV}} = 55.128 \text{mA/V} \quad [1 \text{ mark}]$$

$$r_{\pi 4} = \frac{\beta V_T}{I_O} \quad [1 \text{ mark}]$$

$$r_{\pi 4} = 150 \left(\frac{26 \text{mV}}{1.433 \text{mA}}\right) = 2.721 \text{k}\Omega \quad [1 \text{ mark}]$$

Question 2 [20 marks]**Answers:**

Q2a(i) Design the circuit such that $I_3 = 400 \mu\text{A}$ and $V_{CE1} = V_{CE2} = 10 \text{ V}$. [5 marks]

Neglect the base currents;

$$I_1 = I_3 = 400 \mu\text{A}$$

$$\text{Using KVL, } R_1 = (V^+ - V_{BE4} - V^-) / I_1$$

$$R_1 = (15 - 0.7 - (-15)) / 0.4\text{m} = \underline{\underline{73.25 \text{ k}\Omega}} \quad [1, 1, 0.5]$$

$$\text{As } V_{CE1} = 10 \text{ V}; V_{C1} = V_{CE1} - V_E = 10 - 0.7 = 9.3 \text{ V}$$

$$R_C = (V^+ - V_{C1}) / I_{C1} = (15 - 9.3) / (400\mu/2) = \underline{\underline{28.5 \text{ k}\Omega}} \quad [1, 1, 0.5]$$

Q2a(ii) Determine A_d and $CMRR_{dB}$ for a one-sided output at v_{O2} . A_{cm} is given as -0.113 .

[5 marks]

Find r_π ,

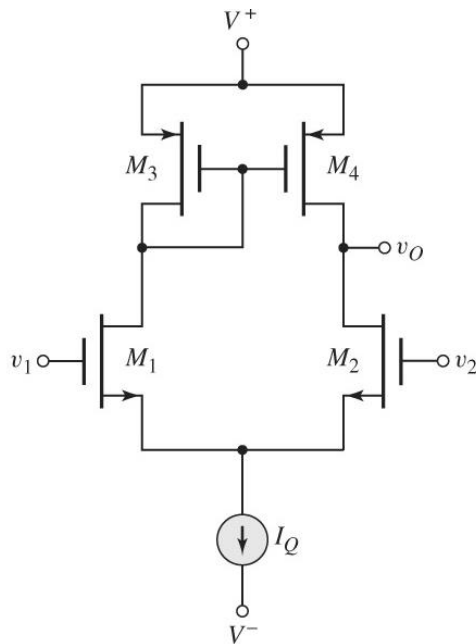
$$r_\pi = \beta v_T / I_{CQ} = (100)(0.026) / 200\mu = \underline{\underline{13 \text{ k}\Omega}} \quad [0.5, 0.5]$$

$$A_d = \beta R_C / 2(r_\pi + R_B)$$

$$= (100)(28.5\text{k}) / 2(13\text{k} + 10\text{k}) = \underline{\underline{62}} \quad [1, 1]$$

$$\text{Thus, } CMRR_{dB} = 20 \log_{10} (62/0.113) = \underline{\underline{54.8 \text{ dB}}} \quad [1, 1]$$

Q2b(i) Draw an improved diff-amp for the circuit in **Figure 3**. Use **Table 1** for the transistors specification. **[4 marks]**



M3 and M4 placement [2]

PMOS type [2]

Q2b(ii) Calculate the minimum power supply voltages if the common input voltage is to be in the range of ± 3 V. Assume symmetrical supply voltages.

[6 marks]

$$i_{D3} = K_p (v_{SG3} + V_{TP})^2 \quad [2]$$

$$0.5\text{m}/2 = 0.25\text{m} (v_{SG3} - 0.4)^2$$

$$v_{SG3} = \underline{\underline{1.4 \text{ V}}} \quad [1]$$

Then, assuming that $v_{SG3} = v_{GS1}$,

$$v_{DS1}(\text{sat}) = v_{GS1} - V_{TN} = 1.4 - 0.4 = \underline{\underline{1.0 \text{ V}}} \quad [2]$$

$$v_{CM} = V_O - v_{DS1}(\text{sat}) + v_{GS1}$$

$$3 = (V^+ - 1.4) - 1.0 + 1.4 \Rightarrow \underline{\underline{V^+ = 4 \text{ V and } V^- = -4 \text{ V}}} \quad [1]$$

Question 3 [20 marks]

Answers:

Q3(a) $I_1 = (V^+ - V_{BE7} - V^-) / (R_1)$ [1]
 $= (10 - 0.7 - (-10)) / (19.3k) = 1 \text{ mA}$ [1]
 $I_Q = I_1 / (1 + 2/\beta) = 0.990 \text{ mA}$ [2]
 $I_{C2} = I_Q / 2 = 0.495 \text{ mA}$ [2]
 $v_{O2} = V^+ - I_{C2} R_C = 10 - (0.495m)(10k) = 5.05 \text{ V}$ [2]
 $I_{R4} = (v_{O2} - 2 V_{BE(on)}) / (R_4)$
 $= (5.05 - 1.4) / (11.5k) = 0.3173 \text{ mA}$ [0.5]
 $I_{R5} \approx I_{R4}$ (neglecting base currents) = 0.3173 mA [0.5]
 $v_{O3} = V^+ - I_{R5} R_5 = 10 - (0.348m)(5k) = 8.413 \text{ V}$ [1]

Q3(b) Using $I_{C2} = 0.495 \text{ mA}$, $I_{R4} = 0.3173 \text{ mA}$:
 $A_{d1} = (g_{m2} / 2)(R_C \parallel R_{i2})$
 $g_{m2} = I_{C2} / V_T = (0.495mA)/(26mV) = 19 \text{ mA/V}$ [1]
 $r_{\pi4} = \beta V_T / I_{R4} = (200 \times 26m) / (0.3173m) = 16.388 \text{ k}\Omega$ [1]
 $r_{\pi3} \approx \beta r_{\pi4} = 200 \times 16.388k = 3277.6 \text{ k}\Omega$ [1]
 $R_{i2} = r_{\pi3} + (1 + \beta) r_{\pi4}$ [1]
 $= 3277.6k + (201)(16.388k) = 6571.59 \text{ k}\Omega$ [1]
 $A_{d1} = (19m/2)(10k \parallel 6571.59k) = 94.85$ [1]
 $A_{v2} \approx (I_{R4} / 2V_T) R_5 = (0.3173 / (2 \times 26m))(5k) = 30.5$ [1]
 $A_3 \approx 1$ (Output stage assume gain = 1) [1]
 $A_d = A_{d1} A_{v2} A_3$ [1]
 $= 94.85 \times 30.5 \times 1 = 2893.8$ [1]

OR

Q3(a) $I_1 = (V^+ - V_{BE7} - V^-) / (R_1)$ [1]
 $= (10 - 0.7 - (-10)) / (19.3k) = 1 \text{ mA}$ [1]
 $I_Q \approx I_1$ [Since $\beta = 200 \gg 1$] = 1 mA [2]
 $I_{C2} = I_Q / 2 = 0.5 \text{ mA}$ [2]
 $v_{O2} = V^+ - I_{C2} R_C = 10 - (0.5m)(10k) = 5 \text{ V}$ [2]
 $I_{R4} = (v_{O2} - 2 V_{BE(on)}) / (R_4)$
 $= (5 - 1.4) / (11.5k) = 0.313 \text{ mA}$ [0.5]
 $I_{R5} \approx I_{R4}$ (neglecting base currents) = 0.313 mA [0.5]
 $v_{O3} = V^+ - I_{R5} R_5 = 10 - (0.313m)(5k) = 8.44 \text{ V}$ [1]

Q3(b) Using $I_{C2} = 0.5 \text{ mA}$, $I_{R4} = 0.313 \text{ mA}$:
 $A_{d1} = (g_{m2} / 2)(R_C \parallel R_{i2})$
 $g_{m2} = I_{C2} / V_T = (0.5mA)/(26mV) = 19.23 \text{ mA/V}$ [1]
 $r_{\pi4} = \beta V_T / I_{R4} = (200 \times 26m) / (0.313m) = 16.613 \text{ k}\Omega$ [1]
 $r_{\pi3} \approx \beta r_{\pi4} = 200 \times 16.613k = 3322.6 \text{ k}\Omega$ [1]
 $R_{i2} = r_{\pi3} + (1 + \beta) r_{\pi4}$ [1]
 $= 3322.6k + (201)(16.613k) = 6661.8 \text{ k}\Omega$ [1]
 $A_{d1} = (19.23m/2)(10k \parallel 6661.8k) = 96$ [1]
 $A_{v2} \approx (I_{R4} / 2V_T) R_5 = (0.313m / (2 \times 26m))(5k) = 30$ [1]
 $A_3 \approx 1$ (Output stage assume gain = 1) [1]
 $A_d = A_{d1} A_{v2} A_3$ [1]
 $= 96 \times 30 \times 1 = 2880$ [1]

Question 4 [20 marks]

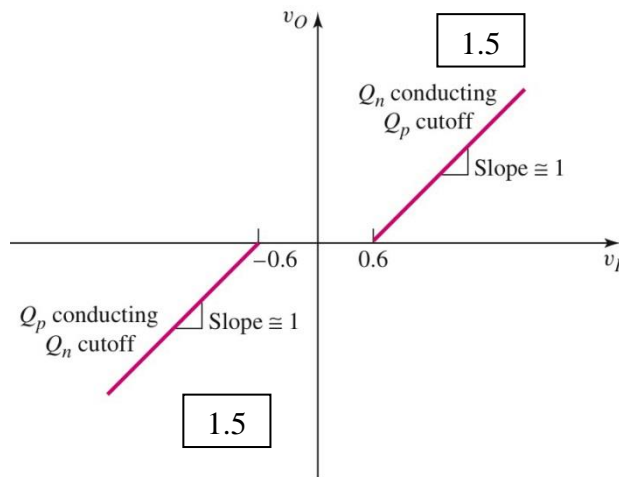
Answers:

Q4a(i)

Figure 4(a) - Approximate class-B output stage [1]

Figure 4(b) - Class-AB output stage [1]

Q4a(ii)



Q4a(iii)

$$i_{Cn} = i_{Cp} = I_S e^{\frac{V_{BB}}{2V_T}} \quad \boxed{0.5}$$

$$i_{Cn} = (4 \times 10^{-13}) \left(e^{\left[\frac{1.2}{(2)(0.026)} \right]} \right) = 4.210 \text{ mA} \quad \boxed{1}$$

$$P_{Qn} = P_{Qp} = v_{CE} i_C \quad \boxed{0.5}$$

$$v_{CE} = 12 \text{ V}$$

$$P_Q = (12)(4.210 \text{ m}) = 50.52 \text{ mW} \quad \boxed{1}$$

$$v_{O(\max)} = 12 \text{ V} \quad \boxed{1}$$

$$P_{L(\max)} = \frac{1}{2} \frac{V_p^2}{R_L} = (0.5) \left(\frac{12^2}{100} \right) = 0.72 \text{ W} \quad \boxed{1}$$

Question 4(b) [10 marks]

To calculate I_{C16} , need to determine I_{C13B}

$$I_{C13B} = 0.75 I_{C12} = (0.75)(0.3\text{m}) = 0.225 \text{ mA} \quad [1 \text{ mark}]$$

$$I_{C17} = I_{C13B} = 0.225 \text{ mA} \quad [1 \text{ mark}]$$

$$I_{C16} \cong I_{E16} = I_{B17} + I_{R9} = I_{C17} / \beta + (I_{C17}R_8 + V_{BE17}) / R_9 \quad [1 \text{ mark}]$$

$$I_{C16} = (0.225\text{m}/200) + ([0.225\text{m} \times 100 + 0.7] / 50\text{k})$$

$$I_{C16} = 1.125\mu + 14.45\mu = 15.575 \mu\text{A} \quad [1 \text{ mark}]$$

$$R_{b16} = r_{pi16} + (1+B)[R_9 \parallel R_{b17}] \quad [1 \text{ mark}]$$

$$R_{b17} = r_{pi17} + (1+B)R_8 \quad [1 \text{ mark}]$$

$$R_{pi17} = B.VT/I_{C17} = (200)(26\text{m})/0.225\text{m} = 23.11 \text{ kOhm} \quad [1 \text{ mark}]$$

$$R_{pi16} = B.VT/I_{C16} = (200)(26\text{m})/15.575\mu = 333.868 \text{ kOhm} \quad [1 \text{ mark}]$$

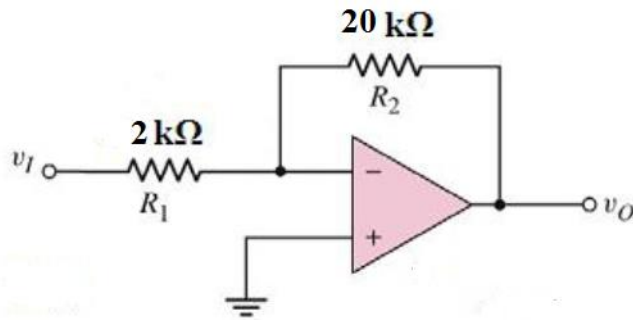
$$\text{So } R_{b17} = 23.11\text{k} + (201)100 = 43.21\text{kOhm} \quad [1 \text{ mark}]$$

$$50\text{k} \parallel 43.21\text{k} = 23.17\text{k}$$

$$\text{So } R_{b16} = 333.868 + (201)(50\text{k} \parallel 43.21\text{k}) = 4.993 \text{ MOhm} \quad [1 \text{ mark}]$$

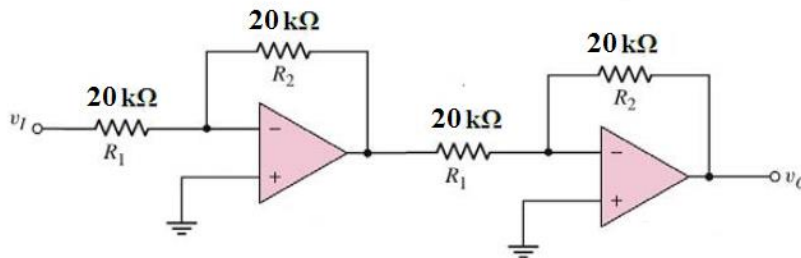
Question 5 [20 marks]

Question 5(a) [8 marks]



- (i) $A_v = -R_2/R_1 = -10$
 $R_1 = R_2/10 = 20k/10 = 2k\Omega$ [1.5 marks]

Correct inverting configuration structure [1.5 marks]



- (ii) $A_v = -R_2/R_1 = -1$
 $R_1 = R_2/1 = 20k/1 = 20k\Omega$ [2 marks]

Correct inverting configuration structure [2 marks]

Cascade inverting for 1st stage and 2nd stage [1 mark]

Question 5(b) [12 marks]

$R_2/R_1 = 80k/20k = 4$ [1 mark]

$R_4/R_3 = 85k/20k = 4.25$ [1 mark]

$V_o = [1+4][4.25/1+4.25]v_{I2} - 4v_{I1} = 4.048v_{I2} - 4v_{I1}$ [2 marks]

$= 4.048(v_{cm}-v_d/2) - 4(v_{cm}+v_d/2)$
 $= 0.048v_{cm} - 4.024v_d$ [2 marks]

Hence, $A_d = 4.024$ [2 marks]

$A_{cm} = 0.048$ [2 marks]

And $CMRR = 20 \cdot \text{Log}(4.024/0.048) = 38.47 \text{ dB}$ [2 marks]